

## CHAPTER SIX

### MONTHLY FLOW MODELS

In this chapter, seven monthly streamflow generation models are described with the basic concepts and some important modifications. These models are Thomas - Fiering model, Disaggregation model, Two-Tier model, method of fragments, etc. The modifications will mainly be concerned with the preservation of skewness coefficient for all these models except method of fragments. Monthly flows are first generated using a Thomas-Fiering monthly model and then adjusted against the annual flow series obtained from Markov models.

#### 6.1 REMOVAL OF SEASONALITY

Seasonality in the monthly flows,  $Q_{1,j}$ , can be modelled using a harmonic function. The periodic component in the mean can be estimated from

$$\mu_j = \mu + \sum_{k=1}^{\omega/2} (A_k \cos(2\pi jk/\omega) + B_k \sin(2\pi jk/\omega)) \quad \text{..... (6.1.1)}$$

in which

$$A_k = 2/\omega \sum_{j=1}^{\omega} \bar{Q}_j \cos(2\pi jk/\omega) \quad \text{..... (6.1.1a)}$$

$$B_k = 2/\omega \sum_{j=1}^{\omega} \bar{Q}_j \sin(2\pi jk/\omega) \quad \text{..... (6.1.1b)}$$

$$\bar{Q}_j = 1/n \sum_{i=1}^n Q_{i,j} \quad \text{..... (6.1.1c)}$$

$$\mu = 1/\omega \sum_{j=1}^{\omega} \bar{Q}_j \quad \dots\dots\dots (6.1.1d)$$

$n$  = number of years of flow records; and  $\omega = 12$  for monthly flows. Similarly, the periodic component in the standard deviation can be estimated from

$$\sigma_j = \sigma + \sum_{k=1}^{\omega/2} (A'_k \cos(2\pi jk/\omega) + B'_k \sin(2\pi jk/\omega)) \quad \dots\dots\dots (6.1.2)$$

in which  $A'_k$ ,  $B'_k$ , and  $\sigma$  can be obtained from Eq. (6.1.1a), (6.1.1b) and (6.1.1d) by replacing  $\bar{Q}_j$  by  $S_j$  which is obtained from

$$S_j = [1/(n-1) \sum_{i=1}^n (Q_{i,j} - \bar{Q}_j)^2]^{1/2} \quad \dots\dots\dots (6.1.3)$$

The periodic components in the means and variances are removed from  $Q_{i,j}$  by

$$q'_{i,j} = (Q_{i,j} - \mu_j) / \sigma_j \quad \dots\dots\dots (6.1.4)$$

in which  $q'_{i,j}$  is stationary in the mean and variance. The mean and standard deviation of  $q'_{i,j}$  will not exactly equal 0 and 1, respectively, and a further transformation is required:

$$q''_{i,j} = (q'_{i,j} - \bar{q}_j) / s_j \quad \dots\dots\dots (6.1.5)$$

in which  $\bar{q}_j$  and  $s_j$  = the mean and standard deviation of  $q'_{i,j}$ , respectively corresponding to month  $j$ . Roener and Yevjevich(1966) called series  $q''_{i,j}$  the standardized fitted series.

Alternatively, for monthly flows, it is convenient to use  $\bar{Q}_j$  and  $S_j$  as the estimates of  $\mu_j$  and  $\sigma_j$  to remove the periodicities in

the mean and variance

$$q_{1,j} = (Q_{1,j} - \bar{Q}_j) / S_j \quad \dots\dots\dots (6.1.6)$$

This method is referred to as the non parametric method of cyclic standardization (Svanidze, 1964) and the series  $q_{1,j}$  is called the standardized series. Srikanthan and McMahon (1982) found that there was little difference in the correlograms of  $q'_{1,j}$  and  $q_{1,j}$ . Because of these observations and computational simplicity, the cyclic standardization is preferred to harmonic analysis in removing the seasonalities.

## 6.2 THOMAS-FIERING MODEL

This model takes into account the seasonality in the monthly means, standard deviations and lag one autocorrelation coefficients automatically in the generating equation which is given below

$$Q_{1,j} = \bar{Q}_j + b_j (Q_{1,j-1} - \bar{Q}_{j-1}) + t_{1,j} S_j (1 - r_j^2)^{1/2} \quad (6.2.1)$$

and

$$Q_{1,1} = \bar{Q}_1 + b_1 (Q_{1-1,12} - \bar{Q}_{12}) + t_{1,1} S_1 (1 - r_1^2)^{1/2} \quad (6.2.2)$$

in which  $b_j$  is the regression coefficient for estimating the flows in the  $j^{th}$  month from the  $(j-1)^{th}$  month,  $t_{1,j}$  is a random normal deviate with zero mean and unit variance,  $S_j$  is the standard deviation of the flows in the  $j^{th}$  month and  $r_j$  is the correlation coefficient between the historical flows of the  $j^{th}$  and  $(j-1)^{th}$  months.

### 6.2.1 Estimation of Parameters

Let  $Q_{1,j}$  ;  $i = 1, 2, 3, \dots, N$  ;  $j = 1, 2, 3, \dots, 12$  be observed discharge in the  $j^{th}$  month of the  $i^{th}$  water year of a set of

available data of N years then the parameters of the model in the  $j^{th}$  month are computed from the following relationships.

1. the mean,

$$\bar{Q}_j = (1/N) \sum_{i=1}^N Q_{i,j} \quad \dots\dots\dots (6.2.3)$$

2. the standard deviation

$$S_j = [1/(N-1) \sum_{i=1}^N (Q_{i,j} - \bar{Q}_j)^2]^{1/2} \quad \dots\dots\dots (6.2.3a)$$

3. the correlation coefficient,

$$r_j = \frac{\sum_{i=1}^N (Q_{i,j} - \bar{Q}_j)(Q_{i,j-1} - \bar{Q}_{j-1})}{[\sum_{i=1}^N (Q_{i,j} - \bar{Q}_j)^2 \sum_{i=1}^N (Q_{i,j-1} - \bar{Q}_{j-1})^2]^{1/2}} \quad \dots\dots\dots (6.2.4)$$

4. the regression coefficient,

$$b_j = r_j S_j / S_{j-1} \quad \dots\dots\dots (6.2.5)$$

In Eq. (6.2.4) and Eq. (6.2.5), when  $j=1$  the index  $j-1$  should be 12 instead of 0.

## 6.2.2 Modifications to Account for the Skewness

Yagil (1963) has shown that the regression equation of the above form does preserve the mean, the variance and the correlation between the flows of successive monthly streamflow sequences. Eq. (6.2.1) and (6.2.2) apply to the cases where the monthly flows are normally distributed. In order to take into account the skewness, Thomas and Fiering (1962) replaced the random component

$t_{1,j}$  by  $\epsilon_{1,j}$ , which is defined as

$$\epsilon_{1,j} = \{((1+\gamma(\epsilon_j)t_{1,j}/6-\gamma(\epsilon_j)^2/36)^3-1)2/\gamma(\epsilon_j)\} \dots\dots (6.2.6)$$

where the skewness of  $\epsilon_{1,j}$  denoted by  $\gamma(\epsilon_j)$  is related to the skewness of  $Q_{1,j}$  denoted by  $\gamma_j$  by

$$\gamma(\epsilon_j) = (1-\rho_j^3)\gamma_j/(1-\rho_j^2)^{3/2} \dots\dots (6.2.7)$$

With  $\epsilon_{1,j}$  as the random component. Eq. (6.2.1) and (6.2.2) may be used to generate synthetic events that will resemble the historic events in terms of means, standard deviations, skewnesses and lag one autocorrelations. The flows will be approximately distributed as Gamma. Matalas (1967b) proposed a technique for generating flows which are exactly distributed as Gamma, but only for particular values of  $\gamma_j$  and is limited to  $\gamma_j < 2(2)^{1/2}$ .

### 6.3 TWO - TIER MODEL

Harms and Campbell (1967) extended the Thomas-Fiering model for the sequential generation of monthly streamflows, so as to preserve the monthly as well as annual parameters. In this method, the monthly flows are generated by a Thomas-Fiering monthly model using Eq. (6.2.1) and (6.2.2). The annual streamflow sequence can be generated by an appropriate generation model. If  $Q_i$  is the annual streamflow volume for the year  $i$ , then the adjusted monthly flow volumes are given by

$$Q'_{1,j} = Q_i Q_{1,j} / \sum_{j=1}^{12} Q_{1,j} \quad ; \quad j = 1, 2, \dots, 12 \quad \dots\dots (6.3.1)$$

$Q'_{1,j}$  = adjusted monthly generated flows

$Q_{1,j}$  = unadjusted monthly generated flows

$i$  = year and  $j$  = month

This adjustment procedure preserves the annual parameters of the streamflow sequences at a slight expense of the monthly parameters.

Although the results presented by Harms and Cambell suggest that the model works well, Srikanthan and McMahon (1982) have found that the model distorts seasonal monthly parameters. To improve the seasonal monthly parameters, the Two-Tier model was modified as follows. The annual series obtained from an annual model and the series obtained by summing the monthly flows from the Thomas-Fiering monthly model were ranked separately. The monthly flows for each twelve month period were then adjusted using Eq. (6.3.1) against the annual flows having the same rank as the summed monthly flows. The adjusted monthly flows were then rearranged according to the original sequencing of the annual series. This modified procedure improved the seasonal parameters, especially the means and standard deviations, but had little influence on the skewness and correlation. In addition the method of adjusting monthly data does not allow the monthly serial correlation coefficient from the end of one year to the beginning of the next to be preserved.

#### 6.4 DISAGGREGATION PROCESS

The disaggregation model of Valencia and Shaake (1973) for a single site takes the form

$$X = AY + Z \quad \dots\dots\dots (6.4.1)$$

where X is a (12x1) matrix of monthly flows, Y is the annual flow, A is a (12x1) matrix of constant coefficients and Z is a (12x1) matrix of residuals which have zero mean and are uncorrelated with Y. The elements of matrix X are assumed to be circularly stationary and ergodic; this implies that the aggregation of the lower level

events or the series Y is stationary.

The random component matrix Z may be generated by the relation of

$$Z = BV \quad \dots\dots\dots (6.4.2)$$

where V is a (12x1) matrix of independent, identically distributed normal deviates and B is a (12x12) coefficient matrix in order to preserve the covariance and cross-covariance structure of the residuals. The matrices A and B can be obtained from

$$A = S_{XY} S_{YY}^{-1} \quad \dots\dots\dots (6.4.3)$$

$$\begin{aligned} BB^T &= S_{ZZ} \quad \dots\dots\dots (6.4.4) \\ &= S_{XX} - S_{XY} S_{YY}^{-1} S_{YX} \end{aligned}$$

$$\text{where } S_{XX} = E[XX^T] \quad \dots\dots\dots (6.4.5)$$

$$S_{XY} = E[XY] \quad \dots\dots\dots (6.4.6)$$

$$S_{YX} = E[YX^T] \quad \dots\dots\dots (6.4.7)$$

$$S_{YY} = E[YY^T] \quad \dots\dots\dots (6.4.8)$$

$$\text{and } S_{ZZ} = E[ZZ^T] \quad \dots\dots\dots (6.4.9)$$

$E[X]$  denotes the expectation of X.

The coefficient matrices A and B preserve the first and second moments of the historical annual and monthly flows. The solution of (6.4.4) requires that the matrix  $BB^T$  be positive semi definite. Valencia and Schaake (1973) showed that if  $BB^T$  is obtained by means of the least square estimator of sample covariances, then  $BB^T$  is positive semi definite. The techniques usually used to solve for B given  $BB^T$  are the principal component analysis (Anderson, 1960) or the Cholesky decomposition of  $BB^T$  (Healy, 1968)

#### 6.4.1 Cholesky Decomposition of $BB^T$

In this method, the matrix B is assumed to be lower-triangular and the elements  $b_{i,j}$  of B are obtained from the following recursive relationships:

$$b_{1,j} = 0, \quad j > 1 \quad \dots\dots\dots (6.4.10)$$

$$b_{1,1} = c_{1,1}^{1/2} \quad \dots\dots\dots (6.4.11)$$

where  $c_{1,j}$  is the element of matrix  $C = BB^T$ . The remaining elements in the first column of B are given by

$$b_{1,1} = c_{1,1}/b_{1,1} \quad \dots\dots\dots (6.4.12)$$

The  $j^{th}$  diagonal element is obtained from

$$b_{j,j} = [c_{1,j} - \sum_{k=1}^{j-1} b_{j,k}^2]^{1/2} \quad j = 2, 3, \dots, w \quad \dots\dots (6.4.13)$$

The solution is complete when  $j = w$ . Otherwise, the other elements of column  $j$  of B are computed from

$$b_{i,j} = [c_{1,j} - \sum_{k=1}^{j-1} b_{i,k} b_{j,k}] / b_{j,j}, \quad i = j+1, j+2, \dots, w \quad \dots\dots\dots (6.4.14)$$

#### 6.4.2 Wilson-Hilferty Transformation

To generate skewed monthly flows is as follows. Expanding Eq. (6.4.1) and assuming B to be a lower triangular matrix, for month  $j$

$$x_j = a_j Y + \sum_{k=1}^j b_{j,k} v_k \quad \dots\dots\dots (6.4.15)$$

where  $x_j$ ,  $a_j$ ,  $b_{j,k}$  and  $v_k$  are the elements of  $j^{th}$  row of the matrices X, A, B and V respectively and Y is the annual flow. Assume that the sample values of X and Y are adjusted to have zero mean. Cubing both sides of Eq. (6.4.15) and taking expectations

$$E[x_j^3] = a_j^3 E[y^3] + \sum_{k=1}^j b_{j,k}^3 E[v_k^3] \quad \dots\dots\dots (6.4.16)$$

By dividing both sides of Eq. (6.4.16) by  $\sigma_j^3 \sigma^3$ , one would obtain

$$\gamma/\sigma^3 = (a_j/\sigma_j)^3 \gamma + 1/(\sigma^3 \sigma_j^3) \sum_{k=1}^j b_{j,k}^3 \gamma(v_k) \quad \dots\dots (6.4.17)$$

where  $\sigma_j$  - standard deviation of the j-th monthly flow

$\gamma_j$  - coefficient of skewness of the j<sup>th</sup> monthly flows

$\gamma$  - coefficient of skewness of the annual flows

$\sigma$  - standard deviation of the annual flows

and  $\gamma(v_k)$  - coefficient of skewness of the k<sup>th</sup> random variable in V

The required skewness of the random numbers are given by the following recursive relationship:

$$\begin{aligned} \gamma(v_1) &= \{\sigma_1^3 \gamma_1 - (a_1 \sigma)^3 \gamma\} / b_{1,1}^3 \\ \gamma(v_2) &= \{\sigma_2^3 \gamma_2 - (a_2 \sigma)^3 \gamma - b_{2,1}^3 \gamma(v_1)\} / b_{2,2}^3 \\ &\vdots \\ &\vdots \\ \gamma(v_j) &= \{\sigma_j^3 \gamma_j - (a_j \sigma)^3 \gamma - \sum_{k=1}^{j-1} b_{j,k}^3 \gamma(v_k)\} / b_{j,j}^3 \quad \dots\dots (6.4.18) \end{aligned}$$

It was observed during the computations, that the last term of the matrix B (i.e.  $b_{12,12}$ ) was always zero or very small. Because of this the twelfth random number had little or no effect on the generated streamflows. In other words the flow during month 12 depends only on the annual flow and the previous 11-month flow of a given year. In addition,  $\gamma(v_{12})$  was undefined (or extremely large) because of zero denominator. Consequently, the 12<sup>th</sup> month flows assumes an implied skew given by:

$$\gamma(v_{12}) = [\sigma a_{12} / \sigma_{12}]^3 \gamma + (1/\sigma_{12}^3) \sum_{j=1}^{11} b_{12,j}^3 \gamma(v_j) \quad \dots\dots (6.4.19)$$

## 6.5 METHOD OF FRAGMENTS

Svanidze (1964) which uses the observed monthly flows to

disaggregate the annual flows. This method is referred to as "the method of fragments" (Klemes, 1979, personal communication) and is described below.

In this method, the observed monthly flows are standardized year by year so that the sum of monthly flows in any year equals unity. This is done by dividing the monthly flows in a year by the corresponding annual flow. By doing so, from a record of  $n$  years, one will have  $n$  fragments of yearly monthly flows. The annual flows obtained from any of the annual models can be disaggregated by selecting the fragments at random. This method also has the disadvantage that the correlation between the first month of a year to the last month of the previous year will not be preserved. This procedure was used with annual flows generated from Markov models.

It was found, applying this approach, that the seasonal monthly parameters were not satisfactorily preserved. However, the monthly parameters can be improved by selecting a fragment appropriate to each flow in the annual flow series (Srikanthan and McMahon, 1982). This is done in the following manner.

The annual flows from the historical record (say  $N$  years long) are ranked according to increasing magnitude and  $N$  class  $N$  has no upper limit. The intermediate class limits are obtained by averaging two successive flows in the ranked series. The corresponding fragment are assigned to each class as follows. The fragment obtained from the monthly flows contributing to the smallest annual flows. The fragment obtained from the monthly flows contributing to the smallest annual flow is assigned to class 1, the fragment obtained from the monthly flows corresponding to the second smallest annual flow is assigned the class 2, and so on. The generated annual flows are then checked one by one for the class to which they belong and disaggregated using the corresponding fragment.

## 6.6 FIRST SPOLIA-CHANDER MODEL

Following Young and Pisano (1968), Spolia and Chander (1974) removed the periodicity in monthly streamflow sequences by using the cyclic linear transformation :

$$a_{1,j} = (Q_{1,j} - \bar{Q}_j) / s_j \quad \dots\dots\dots (6.6.1)$$

Since the resulting residual sequence,  $\{a_{1,j}\}$ , is cyclic free, all the elements  $a_{1,j}$  could be considered to belong to the same population. They then proposed an  $m^{\text{th}}$ -order autoregressive model for modelling this residual sequence. Define :

$$u_k = a_{1,j} \quad \dots\dots\dots (6.6.2)$$

where

$$k = 12(i-1)+j, \quad j = 1, \dots, 12 ; \quad i = 1, \dots, n \quad \dots\dots (6.6.3)$$

$n$  being the length of the historical record in years, Then:

$$u_k = \sum_{l=1}^m b_l u_{k-l} + t_k (1-R^2)^{1/2} \quad \dots\dots\dots (6.6.4)$$

in which  $b_l$  is the  $l^{\text{th}}$  regression coefficient and  $R$  is the multiple correlation coefficient. To determine the appropriate order of the autoregressive model employed, they simply applied the Anderson test on the serial correlation coefficient of the residual series. It turned out that either the first-or the second-order model is needed.

The removal of periodicities by means of Eq.(6.6.1) is commonly known as the nonparametric method (Tao et al., 1976). Another alternative is the parametric method also described by Tao et al. who claimed that it is more desirable than the previous one but little difference in the correlograms of both these two methods (Srikanthan and McMahon, 1982). In this study, the nonparametric method is preferred to the parametric method in

removing the seasonalities because of its simplicity. Beside the introduction of the nonparametric method, attempts were also made to modify the model so as to account for the skewness coefficient.

Since only first- and second-order autoregressive models are expected to be required in modelling the residual series, only these are considered in the following. It should first be noticed that the residual series obtained by the removal of periodicities from the monthly sequence is in fact weakly stationary in the sense that it is stationary only in the mean and variance. This implies that the skewness coefficient of the residual series has still seasonality. Therefore, it is more convenient to use the notation  $a_{1,j}$  rather than  $u_k$ .

#### 6.6.1 For the first-order model:

$$a_{1,j} = \rho_1 a_{1,j-1} + t_j (1 - \rho_1^2)^{1/2} \quad \dots\dots\dots (6.6.5)$$

where  $\rho_1$  is the lag one autocorrelation coefficient of the residual series. By cubing and taking the expectation, it follows from Eq. (6.6.5) that :

$$g(t_j) = \{E(a_{1,j}^3) - \rho_1^3 E(a_{1,j-1}^3)\} / (1 - \rho_1^2)^{3/2} \quad (6.6.6)$$

Since

$$E(a_{1,j}^3) = E(Q_{1,j}^3) = g_j \quad \dots\dots\dots (6.6.7)$$

one obtains from Eq. (6.6.6)

$$g(t_j) = (g_j - \rho_1^3 g_{j-1}) / (1 - \rho_1^2)^{3/2} \quad \dots\dots\dots (6.6.8)$$

#### 6.6.2 For the second-order model :

$$a_{1,j} = b_1 a_{1,j-1} + b_2 a_{1,j-2} + t_j (1 - R^2)^{1/2} \quad \dots\dots\dots (6.6.9)$$

Cubing Eq. (6.6.9) and taking the expectation, by noting that the terms :

$$E(a_{1,j-1}a_{1,j-2}t_j^3); E(a_{1,j-2}^2t_j^3); E(a_{1,j-1}^2t_j^3); \text{ and } E(a_{1,j}^2t_j^3)$$

all vanish, one obtains the following expression :

$$g(t_j) = [g_j - b_1^3 g_{j-1} - b_2^3 g_{j-2} - 3b_1^2 b_2 E(a_{1,j-1}^2 a_{1,j-2}) - 3b_1 b_2^2 E(a_{1,j-1} a_{1,j-2}^2)] / (1-R^2)^{3/2} \dots\dots\dots (6.6.10)$$

By neglecting the third moments of  $a_{1,j-1}$  and  $a_{1,j-2}$ , Eq. (6.6.10) reduces to

$$g(t_j) = (g_j - b_1^3 g_{j-1} - b_2^3 g_{j-2}) / (1-R^2)^{3/2} \dots\dots\dots (6.6.11)$$

## 6.7 SECOND SPOLIA-CHANDER MODEL

This model is based on canonical expansions. Canonical expansion was used by Spolia and Chander (1977) as a representation of a stochastic process in the form of a linear combination of uncorrelated random variables. Let  $Q_j$ ,  $j = 1, \dots, 12$ , denoted the streamflow in month  $j$ , then :

$$Q_j = \bar{Q}_j + \sum_{k=1}^{j-1} b_{j,k} C_k + C_j \dots\dots\dots (6.7.1)$$

where  $\{C_j\}$  is a sequence of random variables of zero mean which are uncorrelated with one another, and  $b_{j,k}$  are real coefficients. For the model of Eq.(6.7.1) to preserve the mean, variance and the entire correlation-cross-correlation matrix of the historical monthly streamflows, the variance of  $C_j$  and the coefficients  $b_{j,k}$  must be computed :

$$\text{Var}(C_1) = \text{Var}(Q_1)$$

$b_{1,k} = 1$ , for all  $k=j$ ;  $b_{j,k} = 0$ , for all  $k > j$

$b_{j,1} = \text{Cov}(Q_j, Q_1) / \text{Var}(C_1)$

$$b_{j,k} = [\text{Cov}(Q_j, Q_k) - \sum_{l=1}^{k-1} b_{j,l} b_{k,l} \text{Var}(C_l)] / \text{Var}(C_k), \text{ for } k = 2, 3, \dots, j-1 \quad \dots\dots\dots (6.7.2)$$

and

$$\text{Var}(C_j) = \text{Var}(Q_j) - \sum_{k=1}^{j-1} b_{j,k}^2 \text{Var}(C_k)$$

In order to preserve the skewness coefficient of the historical monthly streamflows, Phien (1979) showed that the third moment of  $C_j$  must be as follows :

$$E(C_1^3) = E(Q_1^3)$$

$$E(C_j^3) = E(Q_j^3) - \sum_{k=1}^{j-1} b_{j,k}^3 E(C_k^3), \quad j > 2 \quad \dots\dots\dots (6.7.3)$$

Knowing the third and second (central) moments of  $C_j$ , one can obtain its skewness coefficient by taking :

$$g(C_j) = E(C_j^3) / [\text{Var}(C_j)]^{3/2} \quad \dots\dots\dots (6.7.4)$$

## 6.8 SEN MODEL

The model proposed by Sen (1978) is a mixture of the stationary lag one autoregressive model and the seasonal Thomas-Fiering model. It can preserve the historical sequences in terms of mean, standard deviation, first serial correlation coefficient between the successive years for the same month and lag-zero cross-correlation coefficient between the successive months of the same year. The model is written as:

$$W_{1,j} = \alpha_j W_{1,j-1} + \beta_j W_{1-1,j} + t_j \quad \dots\dots\dots (6.8.1)$$

where

$$W_{1,j} = Q_{1,j} - \bar{Q}_j \quad \dots\dots\dots (6.8.2)$$

$\alpha_j, \beta_j$  = parameters which reflect the relationships between successive months of the same year and between successive years for the same month, respectively:

$t_j$  = random variable, independent of  $W_{1,j-1}$  and  $W_{1-1,j}$  and having zero mean. When  $\alpha_j = 0$ , Eq.(6.8.1) gives the lag-one autoregressive (Markov) model, and when  $\beta_j = 0$ , it reduces to that of Thomas and Fiering(1962).

Besides the mean,  $\bar{Q}_j$ , and the standard deviation,  $S_j$ , the other model parameters and related constants are as follows:

1. Lag-one serial correlation:

$$\rho_j(1) = \sum_1 (W_{1,j} W_{1-1,j}) / (\sum_1 W_{1,j}^2)^{1/2} \quad \dots\dots\dots (6.8.3)$$

2. Lag-zero cross-correlation coefficient :

$$\rho_{j,j-1}(0) = \sum_1 (W_{1,j-1} W_{1,j}) / [\sum_1 (W_{1,j-1}^2) (\sum_1 W_{1,j}^2)]^{1/2} \quad (6.8.4)$$

3. Lag-one cross-correlation coefficient :

$$\rho_{j,j-1}(1) = \sum_1 (W_{1-1,j} W_{1,j-1}) / [\sum_1 (W_{1-1,j}^2) (\sum_1 W_{1,j-1}^2)]^{1/2} \quad \dots\dots\dots (6.8.5)$$

4. Model parameters:

$$\alpha_j = (S_j / S_{j-1}) [\rho_{j,j-1}(0) - \rho_j(1) \rho_{j,j-1}(1)] / [1 - \rho_{j,j-1}^2(1)] \quad \dots\dots\dots (6.8.6)$$

$$g_j = \frac{\rho_j(1) - [\rho_{j,j-1}(0)\rho_{j,j-1}(1)]}{[1 - \rho_{j,j-1}^2(1)]} \dots\dots\dots (6.8.7)$$

5. Variance of the random variable :

$$\text{Var}(t_j) = S_j^2 - S_j^2 \frac{[\rho_{j,j-1}^2(0) - 2\rho_j(1)\rho_{j,j-1}(0)\rho_{j,j-1}(1) + \rho_j^2(1)]}{[1 - \rho_{j,j-1}^2(1)]} \dots\dots\dots (6.8.8)$$

To preserve the skewness coefficient of each historical month of each historical monthly sequence, the random variable  $t_j$  must have a skewness coefficient which is determined below. Cubing Eq. (6.8.1) and taking the expectation, one obtains:

$$E(t_j^3) = g_j S_j^3 - \alpha_j^3 S_j^3 g_{j-1} - \beta_j^3 S_j^3 g_j - 3\alpha_j^2 \beta_j E[W_{1,j-1}^2 W_{1-1,j}] + 3\alpha_j \beta_j^2 E[W_{1,j-1} W_{1-1,j}^2] \dots\dots\dots (6.8.9)$$

If the expectation on the right-hand side are neglected, Eq. (6.8.9) reduces to :

$$E(t_j^3) = g_j S_j^3 - \alpha_j^3 S_j^2 g_{j-1} - \beta_j^3 S_j^3 g_j \dots\dots\dots (6.8.10)$$

Finally, the skewness coefficient of  $t_j$  is determined by dividing its third moment by  $[\text{Var}(t_j)]^{3/2}$

## 6.9 APPLICATION FOR ACTUAL DATA

Using the monthly models with modification, 1000 years of streamflows were generated for each river. The various parameters of the generated monthly flows from each model were estimated and given in Table 6.1-6.10. The following symbols are used to denote the parameter obtained from the historic and generated sequences.

Hist. - Historical values

- TF - Thomas-Fiering monthly model
- TT - Two-Tier model using the annual flows from Markov model
- TIM - Modified Two-Tier model using the annual flows from a Markov model
- FM - Method of Fragments using the annual flows from a Markov model
- FMM - Modified Method of Fragments using the annual flows from a Markov model
- FSC - First Spolia-Chander monthly model
- SSC - Second Spolia-Chander monthly model
- SEN - Sen monthly model

## 6.10 DISCUSSION OF RESULTS

The statistical parameters for comparison are the central moments (mean, standard deviation and skewness coefficient) and the lag one autocorrelation coefficients. They are computed for each 1000 years of generated sequences. Based on the results in Table 6.1 to 6.10 the models are classified into three groups and the performance of the models with respect to the rivers in each of these groups are discussed below.

### 6.10.1 Thomas-Fiering and Sen Models

Although, Thomas-Fiering model is a very old technique for generated streamflows, it has been favourably used due to its simplicity in form and it can be preserved well the seasonal monthly parameters. From Table 6.1 to 6.10 are shown that the both models give similar results for the mean, standard deviation and the lag-one autocorrelation coefficient for most of the rivers. For the skewness coefficient, both models can preserve for most of the rivers except a few cases. The Thomas-Fiering model results in

positive skewness where as the historical value is negative in August for Nan river and overestimates the skewness in February and March for Nam Mae Taeng. The Sen model overestimates the skewness in April and March for Ping River. For both models, maximum events are more than the historic records except a few cases while the minimum events are smaller than those from historical records. A small amount of zero flows were generated for most of the moments for the both models, which the maximum being 23.8 % for Thomas-Fiering model in March for Nam Mae Khan and 25.9 % for Sen model in April for Wang River.

#### 6.10.2 Disaggregation process, Two-Tier model and Method of Fragments

The advantage of using the Two-Tier model and method of fragments for a single site is that they are simple and can be applied to almost all rivers. The modified disaggregation scheme does not preserve the skewness of the last month of flow and its use is limited in certain cases where the skewness of the random variables obtained from Eq.(6.4.18) becomes large ( $> 10$ ), Srikanthan and McMahon (1982). From calculations the values of the skewness of the random variables are found to be more than 10, so the disaggregation process can not be applied to generate streamflows sequence for each river. Therefore, the Two-Tier model and method of fragments are adjusted to preserve the annual parameters at the slight expense of the seasonal monthly parameters. It is observed that the Two-Tier and method of fragments preserve the seasonal monthly parameters well for most of rivers except a few cases. So both models should be modified to adjust for the seasonal monthly parameters if there is a large difference from historic records. The maximum and minimum events trend to be similar to the first group but the amount of zero flow is more than the first group.

### 6.10.3 First and second Spolia-Chander model

Inspections from Table 6.1 to 6.10 show that both models presented in this study can preserve all first three moment, i.e. mean, standard deviation and skewness coefficient for most of the rivers except the second Second Spolia-Chander model, which can not preserve the standard deviation and skewness coefficient for Nam Mae Taeng and Nam Mae Chaem. Both models can not preserve the lag-one autocorrelation for all of the rivers. The maximum and minimum events trend to be similar in both groups mentioned above but the amount of zero flow is lower.

### 6.11 SUMMARY

Even though the Thomas-Fiering is an old technique, however, it can preserve the seasonal monthly parameters better than other models and is simple to use. The Sen model can preserve well the seasonal monthly parameters well but the model is complicated. The Two-Tier model and method of fragments can preserve the annual parameters and the seasonal monthly parameters except a few cases, they should be modified to improve the seasonal monthly parameters. The disaggregation model can not be applied for all rivers. First and Second Spolia-Conical models preserve mean, standard deviation and skewness well but fail to preserve lag-one autocorrelation.

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TABLE 6.1 MONTHLY (SEASONAL) PARAMETERS FROM HISTORIC AND GENERATED SEQUENCES FOR PING RIVER, (P.1)

| PARAMETER                                      | MODEL | APRIL  | MAY    | JUNE    | JULY    | AUG.    | SEPT.   | OCT.    | NOV.    | DEC.    | JAN.   | FEB.   | MARCH  |
|------------------------------------------------|-------|--------|--------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|
| Mean<br>$\times 10^6$ cu.m                     | Hist. | 39.183 | 78.707 | 128.864 | 157.625 | 342.784 | 456.860 | 317.834 | 181.883 | 132.195 | 84.366 | 52.851 | 44.890 |
|                                                | TF    | 39.715 | 78.649 | 124.969 | 150.802 | 333.841 | 453.454 | 316.246 | 183.551 | 134.792 | 86.036 | 53.642 | 45.505 |
|                                                | TT    | 43.161 | 85.406 | 126.577 | 155.089 | 339.543 | 468.661 | 333.460 | 191.535 | 142.511 | 90.560 | 56.689 | 47.099 |
|                                                | TTM   | 37.790 | 74.535 | 103.559 | 112.901 | 253.320 | 356.859 | 269.324 | 154.175 | 118.017 | 76.937 | 47.495 | 38.889 |
|                                                | FM    | 44.215 | 82.068 | 126.428 | 161.372 | 338.914 | 474.584 | 333.504 | 187.126 | 136.485 | 88.116 | 57.389 | 50.088 |
|                                                | FMM   | 44.206 | 84.984 | 107.637 | 141.000 | 356.927 | 465.615 | 339.875 | 191.958 | 143.497 | 91.306 | 54.180 | 59.105 |
|                                                | FSC   | 39.705 | 79.192 | 130.600 | 153.781 | 340.031 | 458.272 | 317.667 | 184.064 | 135.211 | 86.060 | 53.417 | 45.123 |
|                                                | SSC   | 38.723 | 77.484 | 121.563 | 159.126 | 332.043 | 470.608 | 320.233 | 182.248 | 133.838 | 84.401 | 50.826 | 43.898 |
|                                                | SEN   | 38.778 | 80.592 | 127.759 | 156.755 | 332.112 | 447.707 | 316.764 | 180.149 | 132.886 | 84.108 | 52.693 | 45.024 |
|                                                | Hist. | 20.779 | 40.936 | 111.755 | 107.265 | 201.970 | 193.662 | 115.942 | 79.913  | 49.795  | 31.933 | 24.746 | 26.720 |
| Standard<br>Deviation<br>$\times 10^6$ cu.m    | TF    | 20.540 | 42.395 | 98.862  | 100.540 | 191.581 | 190.477 | 115.705 | 80.525  | 50.346  | 31.717 | 24.917 | 25.812 |
|                                                | TT    | 29.841 | 56.479 | 84.290  | 87.723  | 154.609 | 201.636 | 152.639 | 97.837  | 69.627  | 45.438 | 32.960 | 30.409 |
|                                                | TTM   | 18.804 | 39.930 | 52.965  | 65.469  | 120.142 | 128.813 | 99.345  | 67.520  | 46.046  | 31.515 | 23.308 | 22.050 |
|                                                | FM    | 27.910 | 45.940 | 85.599  | 103.876 | 150.306 | 206.235 | 138.296 | 91.255  | 55.512  | 38.659 | 30.441 | 34.997 |
|                                                | FMM   | 28.669 | 58.447 | 56.625  | 89.044  | 175.640 | 201.214 | 143.365 | 105.111 | 77.578  | 56.304 | 43.315 | 67.046 |
|                                                | FSC   | 20.631 | 41.800 | 112.356 | 101.538 | 202.075 | 195.185 | 117.272 | 81.131  | 50.381  | 31.406 | 24.835 | 25.636 |
|                                                | SSC   | 21.625 | 40.969 | 86.914  | 109.524 | 180.104 | 198.455 | 109.456 | 76.965  | 48.733  | 31.130 | 21.810 | 23.259 |
|                                                | SEN   | 14.961 | 41.035 | 90.635  | 106.169 | 181.825 | 177.835 | 115.052 | 74.648  | 46.685  | 27.387 | 18.800 | 19.878 |
|                                                | Hist. | 1.259  | 1.083  | 4.291   | 1.948   | 1.854   | 1.099   | 0.733   | 0.989   | 0.670   | 0.431  | 0.833  | 1.406  |
|                                                | TF    | 1.330  | 1.159  | 3.482   | 2.087   | 1.911   | 1.014   | 0.808   | 1.071   | 0.699   | 0.348  | 1.021  | 1.233  |
| Skewness                                       | TT    | 1.860  | 1.763  | 2.532   | 1.373   | 1.215   | 1.623   | 1.401   | 1.366   | 1.209   | 1.160  | 1.347  | 1.331  |
|                                                | TTM   | 1.003  | 1.267  | 2.729   | 2.785   | 2.260   | 1.309   | 0.836   | 0.864   | 0.592   | 0.161  | 0.662  | 0.783  |
|                                                | FM    | 1.264  | 1.796  | 4.760   | 1.831   | 1.234   | 1.189   | 1.354   | 2.098   | 1.337   | 1.281  | 1.365  | 2.171  |
|                                                | FMM   | 0.899  | 0.942  | 1.452   | 1.270   | 1.732   | 0.634   | 1.750   | 1.277   | 1.418   | 1.493  | 2.214  | 2.118  |
|                                                | FSC   | 1.209  | 1.101  | 3.055   | 1.835   | 1.971   | 1.013   | 0.810   | 1.076   | 0.661   | 0.538  | 1.029  | 1.334  |
|                                                | SSC   | 1.317  | 1.046  | 3.391   | 2.015   | 2.340   | 0.663   | 0.466   | 0.718   | 0.267   | 0.184  | 1.415  | 3.884  |
|                                                | SEN   | 2.561  | 1.144  | 3.186   | 1.871   | 1.712   | 0.913   | 0.724   | 1.194   | 0.884   | 0.661  | 1.920  | 4.141  |
|                                                | Hist. | 0.779  | 0.284  | 0.219   | 0.314   | 0.688   | 0.701   | 0.424   | 0.564   | 0.749   | 0.707  | 0.735  | 0.869  |
|                                                | TF    | 0.771  | 0.285  | 0.281   | 0.272   | 0.707   | 0.682   | 0.438   | 0.522   | 0.757   | 0.732  | 0.721  | 0.909  |
|                                                | TT    | 0.428  | 0.550  | 0.496   | 0.224   | 0.690   | 0.566   | 0.498   | 0.680   | 0.793   | 0.776  | 0.800  | 0.932  |
| Lag one<br>auto-<br>correlation<br>coefficient | TTM   | 0.059  | 0.326  | 0.465   | 0.256   | 0.691   | 0.553   | 0.378   | 0.557   | 0.718   | 0.650  | 0.737  | 0.918  |
|                                                | FM    | 0.101  | 0.598  | 0.336   | 0.370   | 0.473   | 0.466   | 0.405   | 0.641   | 0.787   | 0.776  | 0.828  | 0.884  |
|                                                | FMM   | 0.027  | 0.451  | 0.643   | 0.272   | 0.403   | 0.166   | 0.466   | 0.744   | 0.725   | 0.713  | 0.661  | 0.955  |
|                                                | FSC   | 0.566  | 0.566  | 0.595   | 0.581   | 0.575   | 0.585   | 0.609   | 0.554   | 0.603   | 0.614  | 0.570  | 0.594  |
|                                                | SSC   | -0.005 | 0.035  | -0.076  | 0.029   | 0.040   | -0.047  | -0.047  | -0.001  | -0.003  | 0.025  | 0.020  | -0.026 |
|                                                | SEN   | 0.761  | 0.243  | 0.249   | 0.299   | 0.721   | 0.654   | 0.412   | 0.490   | 0.669   | 0.670  | 0.649  | 0.696  |





TABLE 6.2 (CONT.) MONTHLY (SEASONAL) PARAMETERS FROM HISTORIC AND GENERATED SEQUENCES FOR WANG RIVER (W.16)

| PARAMETER                | MODEL | APRIL  | MAY    | JUNE   | JULY    | AUG.    | SEPT.   | OCT.    | NOV.    | DEC.   | JAN.   | FEB.   | MARCH  |
|--------------------------|-------|--------|--------|--------|---------|---------|---------|---------|---------|--------|--------|--------|--------|
| Maximum                  | Hist. | 4.736  | 53.609 | 50.648 | 86.995  | 227.590 | 163.987 | 83.549  | 54.842  | 14.740 | 15.379 | 3.925  | 3.427  |
|                          | TF    | 8.671  | 69.857 | 85.500 | 203.420 | 481.952 | 264.628 | 154.449 | 99.822  | 25.455 | 36.947 | 11.022 | 9.444  |
|                          | TT    | 29.237 | 81.538 | 89.875 | 136.610 | 255.411 | 486.926 | 282.558 | 139.103 | 50.464 | 75.037 | 16.515 | 13.638 |
|                          | TTM   | 7.618  | 61.821 | 65.988 | 131.201 | 253.808 | 181.892 | 99.223  | 72.406  | 18.234 | 32.834 | 10.035 | 8.541  |
|                          | FM    | 19.139 | 49.842 | 86.261 | 153.374 | 382.256 | 415.073 | 208.169 | 122.620 | 49.219 | 38.797 | 9.597  | 11.845 |
|                          | FMM   | 6.144  | 36.282 | 72.316 | 59.021  | 161.980 | 307.316 | 228.890 | 128.865 | 41.002 | 12.632 | 5.889  | 3.217  |
|                          | FSC   | 7.920  | 66.630 | 73.511 | 190.561 | 420.088 | 245.431 | 135.948 | 103.308 | 20.822 | 35.826 | 8.511  | 5.715  |
|                          | SSC   | 9.132  | 53.264 | 73.455 | 180.510 | 443.938 | 280.325 | 117.766 | 91.779  | 30.218 | 28.769 | 7.910  | 7.769  |
| Minimum                  | SEN   | 9.597  | 52.872 | 69.688 | 171.560 | 459.989 | 245.741 | 145.172 | 93.115  | 22.591 | 24.953 | 6.740  | 6.889  |
|                          | Hist. | 0.103  | 1.153  | 0.851  | 1.664   | 12.828  | 25.672  | 16.408  | 4.880   | 2.424  | 1.351  | 0.643  | 0.083  |
|                          | TF    | 0.000  | 1.033  | 0.410  | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000  | 0.000  | 0.000  | 0.000  |
|                          | TT    | 0.000  | 0.439  | 0.234  | 0.000   | 1.066   | 0.000   | 0.000   | 0.000   | 0.000  | 0.000  | 0.000  | 0.000  |
|                          | TTM   | 0.000  | 1.092  | 0.478  | 0.000   | 1.951   | 2.050   | 0.000   | 0.000   | 0.000  | 0.000  | 0.000  | 0.000  |
|                          | FM    | 0.091  | 0.898  | 0.749  | 0.848   | 7.389   | 10.782  | 8.801   | 4.540   | 1.831  | 0.938  | 0.341  | 0.073  |
|                          | FMM   | 0.096  | 1.075  | 0.794  | 2.038   | 11.659  | 22.751  | 16.072  | 4.321   | 2.146  | 1.196  | 0.637  | 0.077  |
|                          | FSC   | 0.000  | 0.000  | 0.000  | 0.000   | 4.266   | 5.914   | 0.000   | 0.000   | 0.000  | 0.000  | 0.000  | 0.000  |
| Percentage of zero flows | SSC   | 0.000  | 0.164  | 4.207  | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 13.563 | 0.000  | 2.397  | 1.858  |
|                          | SEN   | 0.000  | 0.000  | 0.000  | 0.000   | 0.000   | 0.000   | 1.129   | 0.000   | 0.000  | 0.000  | 0.000  | 0.000  |
|                          | Hist. | 0.000  | 0.000  | 0.000  | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000  | 0.000  | 0.000  | 0.000  |
|                          | TF    | 7.700  | 0.000  | 0.000  | 17.000  | 0.100   | 0.300   | 0.300   | 0.300   | 0.900  | 2.300  | 3.100  | 6.500  |
|                          | TT    | 4.800  | 0.000  | 0.000  | 17.400  | 0.000   | 0.100   | 0.200   | 0.200   | 1.400  | 3.500  | 3.200  | 7.600  |
|                          | TTM   | 6.500  | 0.000  | 0.000  | 24.600  | 0.000   | 0.000   | 0.700   | 0.700   | 1.900  | 5.600  | 4.000  | 7.100  |
|                          | FM    | 0.000  | 0.000  | 0.000  | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000  | 0.000  | 0.000  | 0.000  |
|                          | FMM   | 0.000  | 0.000  | 0.000  | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000  | 0.000  | 0.000  | 0.000  |
|                          | FSC   | 0.000  | 3.700  | 0.000  | 0.000   | 0.000   | 0.000   | 0.000   | 0.300   | 0.000  | 2.500  | 1.800  | 0.000  |
|                          | SSC   | 7.700  | 0.000  | 0.000  | 18.200  | 6.300   | 1.500   | 0.800   | 0.900   | 0.000  | 0.900  | 0.000  | 0.000  |
|                          | SEN   | 25.900 | 0.700  | 1.000  | 14.400  | 0.100   | 0.300   | 0.000   | 0.200   | 1.100  | 0.900  | 1.600  | 23.800 |

TABLE 6.3 MONTHLY (SEASONAL) PARAMETERS FROM HISTORIC AND GENERATED SEQUENCES FOR YOM RIVER, (Y.6)

| PARAMETER                                      | MODEL | APRIL  | MAY    | JUNE    | JULY    | AUG.    | SEPT.   | OCT.    | NOV.    | DEC.   | JAN.   | FEB.   | MARCH |
|------------------------------------------------|-------|--------|--------|---------|---------|---------|---------|---------|---------|--------|--------|--------|-------|
| Mean<br>$\times 10^6$ cu.m                     | Hist. | 11.709 | 72.992 | 123.118 | 200.605 | 595.483 | 938.780 | 441.720 | 147.266 | 54.295 | 24.332 | 12.736 | 8.684 |
|                                                | TF    | 11.439 | 72.865 | 122.810 | 191.193 | 597.444 | 948.398 | 442.889 | 151.091 | 56.081 | 24.760 | 12.556 | 8.867 |
|                                                | TT    | 14.179 | 82.569 | 130.914 | 186.067 | 582.197 | 955.269 | 480.601 | 162.476 | 63.933 | 28.405 | 14.747 | 9.869 |
|                                                | TTM   | 11.205 | 66.701 | 99.909  | 116.451 | 410.714 | 658.130 | 371.539 | 124.685 | 51.609 | 23.134 | 12.283 | 8.152 |
|                                                | FM    | 17.417 | 79.180 | 141.808 | 176.996 | 575.232 | 978.070 | 485.499 | 150.896 | 57.490 | 25.588 | 13.641 | 9.410 |
|                                                | FMM   | 22.943 | 99.072 | 184.623 | 165.594 | 554.015 | 892.481 | 523.628 | 160.208 | 60.018 | 27.603 | 12.620 | 8.422 |
|                                                | FSC   | 11.459 | 72.524 | 122.513 | 191.363 | 599.604 | 949.805 | 443.391 | 151.058 | 55.970 | 24.764 | 12.580 | 8.637 |
|                                                | SSC   | 11.424 | 71.854 | 121.563 | 197.944 | 592.560 | 978.827 | 446.197 | 145.402 | 55.736 | 22.685 | 12.007 | 7.599 |
|                                                | SEN   | 10.975 | 74.870 | 126.844 | 204.958 | 588.310 | 929.140 | 445.619 | 145.957 | 54.501 | 23.652 | 12.467 | 8.646 |
|                                                | Hist. | 13.371 | 58.635 | 88.259  | 251.915 | 403.961 | 506.532 | 199.889 | 107.429 | 24.568 | 14.466 | 9.210  | 6.327 |
| Standard<br>Deviation<br>$\times 10^6$ cu.m    | TF    | 11.122 | 60.785 | 91.175  | 215.183 | 396.188 | 511.136 | 198.917 | 111.324 | 24.202 | 13.579 | 8.238  | 5.736 |
|                                                | TT    | 22.976 | 82.779 | 106.945 | 183.199 | 550.274 | 529.815 | 311.097 | 144.238 | 47.339 | 25.134 | 14.484 | 9.466 |
|                                                | TTM   | 12.558 | 54.400 | 69.203  | 131.402 | 289.775 | 346.722 | 184.290 | 89.000  | 21.173 | 13.095 | 8.181  | 5.700 |
|                                                | FM    | 30.798 | 70.194 | 140.726 | 171.779 | 342.467 | 490.726 | 302.552 | 117.960 | 32.852 | 15.828 | 9.006  | 7.045 |
|                                                | FMM   | 37.168 | 71.419 | 164.089 | 195.410 | 322.560 | 471.272 | 298.099 | 112.872 | 33.505 | 21.522 | 7.133  | 5.955 |
|                                                | FSC   | 11.614 | 58.195 | 89.333  | 199.355 | 393.042 | 510.688 | 198.995 | 111.015 | 24.730 | 14.354 | 8.468  | 5.953 |
|                                                | SSC   | 12.263 | 58.013 | 84.763  | 195.939 | 403.478 | 525.692 | 185.108 | 103.081 | 23.430 | 11.867 | 8.382  | 5.203 |
|                                                | SEN   | 8.818  | 57.796 | 86.200  | 228.751 | 392.508 | 483.001 | 206.592 | 108.034 | 23.356 | 12.346 | 8.607  | 6.101 |
|                                                | Hist. | 4.383  | 1.443  | 1.032   | 2.369   | 0.964   | 0.840   | 0.179   | 1.804   | 0.487  | 1.455  | 3.091  | 1.571 |
|                                                | TF    | 4.062  | 1.590  | 1.234   | 2.748   | 1.123   | 0.746   | 0.276   | 2.042   | 1.042  | 1.999  | 3.195  | 1.387 |
| Skewness                                       | TT    | 7.953  | 2.375  | 1.518   | 1.636   | 0.843   | 1.560   | 1.628   | 2.381   | 1.936  | 3.636  | 4.341  | 2.733 |
|                                                | TTM   | 5.382  | 1.501  | 0.938   | 2.569   | 0.944   | 0.902   | 0.306   | 1.326   | 0.219  | 1.847  | 2.568  | 1.545 |
|                                                | FM    | 4.820  | 1.887  | 3.048   | 2.571   | 1.040   | 0.790   | 1.736   | 2.355   | 1.636  | 1.734  | 2.043  | 2.180 |
|                                                | FMM   | 3.699  | 0.850  | 1.588   | 2.397   | 0.536   | 1.109   | 0.919   | 1.987   | 1.834  | 2.241  | 1.682  | 1.187 |
|                                                | FSC   | 3.923  | 1.438  | 1.214   | 2.457   | 1.054   | 0.741   | 0.276   | 2.094   | 0.533  | 1.806  | 3.037  | 1.446 |
|                                                | SSC   | 4.571  | 1.360  | 0.942   | 2.715   | 0.916   | 0.787   | -0.128  | 1.834   | -0.152 | 2.538  | 3.611  | 0.983 |
|                                                | SEN   | 2.859  | 1.506  | 1.023   | 2.376   | 0.947   | 0.814   | 0.187   | 1.909   | 0.855  | 1.390  | 3.787  | 2.043 |
|                                                | Hist. | 0.009  | -0.059 | 0.518   | 0.354   | 0.575   | 0.513   | 0.411   | 0.347   | 0.800  | 0.727  | 0.521  | 0.782 |
|                                                | TF    | 0.028  | -0.071 | 0.537   | 0.361   | 0.572   | 0.514   | 0.430   | 0.305   | 0.837  | 0.778  | 0.545  | 0.752 |
|                                                | TT    | -0.023 | 0.208  | 0.643   | 0.340   | 0.365   | 0.287   | 0.355   | 0.513   | 0.788  | 0.828  | 0.717  | 0.802 |
| Lag one<br>auto-<br>correlation<br>coefficient | TTM   | 0.036  | -0.057 | 0.564   | 0.432   | 0.400   | 0.385   | 0.331   | 0.394   | 0.768  | 0.665  | 0.578  | 0.733 |
|                                                | FM    | 0.032  | 0.189  | 0.707   | 0.242   | 0.440   | 0.358   | 0.437   | 0.475   | 0.831  | 0.787  | 0.667  | 0.748 |
|                                                | FMM   | 0.016  | -0.019 | 0.874   | 0.625   | 0.463   | 0.509   | 0.557   | 0.685   | 0.966  | 0.718  | 0.793  | 0.680 |
|                                                | FSC   | 0.487  | 0.382  | 0.447   | 0.496   | 0.432   | 0.459   | 0.476   | 0.416   | 0.485  | 0.484  | 0.489  | 0.420 |
|                                                | SSC   | -0.034 | 0.029  | -0.062  | 0.032   | 0.071   | -0.035  | -0.040  | 0.025   | -0.021 | 0.021  | 0.010  | 0.005 |
|                                                | SEN   | 0.083  | 0.149  | 0.494   | 0.381   | 0.570   | 0.473   | 0.498   | 0.348   | 0.805  | 0.815  | 0.441  | 0.763 |
|                                                | Hist. | 0.009  | -0.059 | 0.518   | 0.354   | 0.575   | 0.513   | 0.411   | 0.347   | 0.800  | 0.727  | 0.521  | 0.782 |
|                                                | TF    | 0.028  | -0.071 | 0.537   | 0.361   | 0.572   | 0.514   | 0.430   | 0.305   | 0.837  | 0.778  | 0.545  | 0.752 |
|                                                | TT    | -0.023 | 0.208  | 0.643   | 0.340   | 0.365   | 0.287   | 0.355   | 0.513   | 0.788  | 0.828  | 0.717  | 0.802 |
|                                                | TTM   | 0.036  | -0.057 | 0.564   | 0.432   | 0.400   | 0.385   | 0.331   | 0.394   | 0.768  | 0.665  | 0.578  | 0.733 |

TABLE 6.3 (CONT.) MONTHLY (SEASONAL) PARAMETERS FROM HISTORIC AND GENERATED SEQUENCES FOR YOM RIVER, (Y.6)

| PARAMETER                | MODEL | APRIL   | MAY     | JUNE     | JULY     | AUG.     | SEPT.    | OCT.     | NOV.     | DEC.    | JAN.    | FEB.    | MARCH  |
|--------------------------|-------|---------|---------|----------|----------|----------|----------|----------|----------|---------|---------|---------|--------|
| Maximum                  | Hist. | 82.935  | 262.670 | 523.103  | 1157.660 | 1527.352 | 2333.104 | 874.195  | 502.762  | 117.390 | 67.133  | 55.814  | 29.549 |
|                          | TF    | 143.101 | 447.223 | 575.962  | 2288.069 | 3101.591 | 3058.441 | 1254.091 | 997.593  | 218.830 | 137.627 | 92.482  | 48.148 |
|                          | TT    | 397.705 | 695.485 | 768.216  | 1087.936 | 2295.107 | 4943.076 | 2838.207 | 1155.781 | 347.710 | 289.911 | 198.334 | 96.955 |
|                          | TTM   | 136.148 | 406.327 | 472.817  | 1259.090 | 1756.021 | 2269.237 | 938.394  | 562.561  | 135.778 | 118.959 | 63.206  | 39.716 |
|                          | FM    | 261.697 | 496.655 | 1193.191 | 1350.732 | 2570.194 | 3013.937 | 2409.789 | 968.096  | 292.296 | 125.733 | 68.607  | 67.363 |
|                          | FMM   | 193.209 | 274.692 | 635.398  | 852.947  | 1388.711 | 3266.722 | 1531.780 | 805.900  | 255.816 | 106.457 | 53.025  | 25.836 |
|                          | FSC   | 155.010 | 397.581 | 539.786  | 2051.846 | 2525.331 | 3105.334 | 1250.969 | 1036.698 | 156.348 | 130.549 | 90.691  | 41.309 |
|                          | SSC   | 171.696 | 385.741 | 496.614  | 1862.419 | 2406.533 | 3383.892 | 922.287  | 922.220  | 119.153 | 103.910 | 86.285  | 35.419 |
|                          | SEN   | 73.718  | 357.572 | 494.737  | 1847.360 | 2540.723 | 3010.116 | 1138.253 | 949.378  | 192.344 | 102.872 | 90.880  | 54.163 |
| Minimum                  | Hist. | 1.348   | 8.381   | 28.512   | 13.220   | 102.384  | 276.739  | 114.048  | 22.844   | 13.332  | 5.443   | 4.234   | 1.814  |
|                          | TF    | 1.198   | 0.000   | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000   | 0.000   | 1.274   | 0.000  |
|                          | TT    | 0.637   | 0.000   | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000   | 0.000   | 0.385   | 0.000  |
|                          | TTM   | 4.536   | 1.092   | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000   | 0.000   | 1.055   | 0.000  |
|                          | FM    | 0.540   | 2.512   | 8.370    | 4.653    | 24.271   | 108.008  | 48.640   | 14.675   | 7.941   | 2.363   | 1.175   | 0.576  |
|                          | FMM   | 1.357   | 11.130  | 24.900   | 13.077   | 107.496  | 113.847  | 44.356   | 14.449   | 5.185   | 2.117   | 1.647   | 0.706  |
|                          | FSC   | 0.000   | 0.000   | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000   | 0.000   | 1.891   | 0.213  |
|                          | SSC   | 5.080   | 0.000   | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000   | 8.284   | 5.883   | 0.000  |
|                          | SEN   | 0.000   | 0.000   | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000   | 0.541   | 0.000   | 0.000  |
| Percentage of zero flows | Hist. | 0.000   | 0.000   | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000   | 0.000   | 0.000   | 0.000  |
|                          | TF    | 0.000   | 2.400   | 3.200    | 12.300   | 2.000    | 0.400    | 1.000    | 1.000    | 1.200   | 1.400   | 0.000   | 3.300  |
|                          | TT    | 0.000   | 2.300   | 3.600    | 9.900    | 2.500    | 0.200    | 1.000    | 0.900    | 2.200   | 2.000   | 0.000   | 3.800  |
|                          | TTM   | 0.000   | 2.900   | 5.100    | 15.600   | 6.000    | 0.200    | 1.900    | 1.200    | 1.700   | 2.400   | 0.000   | 4.000  |
|                          | FM    | 0.000   | 0.000   | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000   | 0.000   | 0.000   | 0.000  |
|                          | FMM   | 0.000   | 0.000   | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000    | 0.000   | 0.000   | 0.000   | 0.000  |
|                          | FSC   | 0.000   | 0.000   | 0.000    | 0.000    | 0.000    | 0.400    | 1.000    | 0.000    | 0.000   | 0.000   | 0.000   | 0.000  |
|                          | SSC   | 0.000   | 4.900   | 3.100    | 2.600    | 3.300    | 0.600    | 1.400    | 1.400    | 1.000   | 0.000   | 0.000   | 3.500  |
|                          | SEN   | 0.800   | 3.000   | 3.200    | 9.300    | 2.900    | 0.400    | 1.500    | 1.500    | 2.000   | 1.600   | 0.000   | 4.100  |

TABLE 6.4 MONTHLY (SEASONAL) PARAMETERS FROM HISTORIC AND GENERATED SEQUENCES FOR NAN RIVER, (N.1)

| PARAMETER                                      | MODEL | APRIL  | MAY    | JUNE    | JULY    | AUG.    | SEPT.   | OCT.    | NOV.    | DEC.   | JAN.   | FEB.   | MARCH  |
|------------------------------------------------|-------|--------|--------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|
| Mean<br>$\times 10^{-6}$ cu.m                  | Hist. | 27.649 | 62.829 | 175.583 | 453.973 | 821.643 | 638.049 | 236.988 | 103.316 | 56.963 | 36.604 | 22.511 | 19.261 |
|                                                | TF    | 29.294 | 63.470 | 175.738 | 438.328 | 828.400 | 651.229 | 237.978 | 104.627 | 58.529 | 37.905 | 23.450 | 19.964 |
|                                                | TT    | 31.910 | 70.407 | 178.594 | 457.459 | 874.522 | 630.457 | 248.578 | 112.714 | 63.799 | 40.799 | 25.231 | 21.394 |
|                                                | TTM   | 26.131 | 58.203 | 139.098 | 343.121 | 711.471 | 430.770 | 188.656 | 89.723  | 52.100 | 33.231 | 20.550 | 17.409 |
|                                                | FM    | 29.360 | 67.075 | 178.800 | 446.355 | 899.897 | 621.641 | 249.114 | 112.243 | 62.940 | 40.547 | 25.405 | 22.487 |
|                                                | FMM   | 34.344 | 63.677 | 188.671 | 310.941 | 909.109 | 605.246 | 301.269 | 136.047 | 82.006 | 55.966 | 34.905 | 33.683 |
|                                                | FSC   | 28.210 | 63.644 | 175.981 | 440.150 | 825.526 | 649.943 | 237.935 | 104.771 | 58.650 | 37.586 | 22.788 | 19.361 |
|                                                | SSC   | 27.279 | 61.644 | 170.114 | 458.436 | 811.337 | 684.287 | 234.265 | 102.621 | 57.952 | 36.804 | 22.404 | 18.867 |
|                                                | SEN   | 27.504 | 64.223 | 181.502 | 460.387 | 812.418 | 631.000 | 233.946 | 101.992 | 57.019 | 38.800 | 24.056 | 20.594 |
|                                                | Hist. | 19.046 | 43.124 | 132.209 | 314.556 | 281.311 | 415.913 | 128.203 | 45.948  | 25.676 | 17.220 | 11.462 | 10.517 |
| Standard<br>Deviation<br>$\times 10^{-6}$ cu.m | TF    | 19.222 | 44.235 | 136.943 | 300.260 | 273.414 | 414.746 | 128.749 | 46.028  | 25.838 | 17.136 | 11.639 | 10.447 |
|                                                | TT    | 30.062 | 60.206 | 134.362 | 302.464 | 382.155 | 393.108 | 156.728 | 68.093  | 41.683 | 26.706 | 17.232 | 14.668 |
|                                                | TTM   | 18.327 | 40.830 | 92.783  | 224.634 | 274.134 | 296.873 | 105.279 | 41.488  | 23.928 | 16.286 | 10.638 | 9.010  |
|                                                | FM    | 19.165 | 55.679 | 120.228 | 256.470 | 444.823 | 321.141 | 133.859 | 61.707  | 36.049 | 24.405 | 17.136 | 17.290 |
|                                                | FMM   | 16.174 | 46.649 | 96.207  | 116.594 | 367.989 | 300.474 | 165.774 | 76.892  | 39.766 | 25.709 | 18.505 | 19.640 |
|                                                | FSC   | 18.833 | 43.916 | 129.613 | 294.122 | 268.847 | 408.432 | 128.886 | 46.351  | 25.884 | 16.843 | 11.458 | 10.076 |
|                                                | SSC   | 19.548 | 42.996 | 109.235 | 323.121 | 279.882 | 417.610 | 117.382 | 44.005  | 25.456 | 16.931 | 10.508 | 7.847  |
|                                                | SEN   | 17.859 | 43.316 | 128.661 | 323.711 | 285.492 | 401.412 | 115.577 | 40.968  | 23.457 | 16.240 | 11.528 | 10.892 |
|                                                | Hist. | 0.964  | 1.289  | 1.911   | 1.639   | -0.012  | 1.035   | 1.387   | 0.906   | 0.450  | 0.364  | 0.715  | 1.389  |
|                                                | TF    | 0.916  | 1.334  | 2.014   | 1.756   | 0.112   | 0.979   | 1.598   | 0.916   | 0.529  | 0.510  | 0.982  | 1.243  |
| Skewness                                       | TT    | 2.711  | 2.008  | 1.494   | 1.355   | 0.597   | 1.205   | 1.920   | 1.562   | 1.684  | 1.487  | 1.809  | 1.848  |
|                                                | TTM   | 1.460  | 1.553  | 1.520   | 1.773   | 0.102   | 1.194   | 1.317   | 0.884   | 0.257  | 0.166  | 0.339  | 0.445  |
|                                                | FM    | 0.927  | 2.654  | 1.355   | 1.358   | 1.334   | 0.987   | 1.187   | 1.488   | 1.198  | 1.191  | 1.554  | 1.967  |
|                                                | FMM   | 0.301  | 2.273  | 0.195   | -0.048  | 0.453   | 0.481   | 0.466   | 1.414   | 1.067  | 0.383  | 0.600  | 0.392  |
|                                                | FSC   | 0.926  | 1.557  | 1.753   | 1.801   | 0.130   | 1.011   | 1.624   | 0.953   | 0.474  | 0.516  | 0.876  | 1.309  |
|                                                | SSC   | 0.987  | 1.198  | 1.765   | 1.452   | 0.085   | 0.673   | 1.359   | 0.744   | 0.398  | 0.150  | 3.131  | 3.469  |
|                                                | SEN   | 0.774  | 1.169  | 1.825   | 1.501   | 0.020   | 1.083   | 1.364   | 1.107   | 0.683  | 0.951  | 0.911  | 0.896  |
|                                                | Hist. | 0.058  | 0.516  | 0.349   | 0.423   | 0.314   | 0.426   | 0.516   | 0.728   | 0.763  | 0.956  | 0.952  | 0.906  |
|                                                | TF    | 0.048  | 0.497  | 0.352   | 0.429   | 0.338   | 0.413   | 0.543   | 0.705   | 0.774  | 0.965  | 0.945  | 0.938  |
|                                                | TT    | 0.068  | 0.664  | 0.545   | 0.434   | 0.249   | 0.348   | 0.406   | 0.755   | 0.835  | 0.967  | 0.970  | 0.969  |
| Lag one<br>auto-<br>correlation<br>coefficient | TTM   | 0.043  | 0.490  | 0.466   | 0.408   | 0.170   | 0.429   | 0.494   | 0.702   | 0.708  | 0.949  | 0.948  | 0.924  |
|                                                | FM    | 0.045  | 0.632  | 0.315   | 0.365   | 0.296   | 0.265   | 0.553   | 0.703   | 0.899  | 0.973  | 0.972  | 0.950  |
|                                                | FMM   | 0.065  | 0.707  | 0.545   | 0.100   | 0.568   | 0.759   | 0.924   | 0.584   | 0.979  | 0.968  | 0.925  | 0.958  |
|                                                | FSC   | 0.552  | 0.550  | 0.604   | 0.564   | 0.587   | 0.550   | 0.600   | 0.543   | 0.595  | 0.602  | 0.559  | 0.582  |
|                                                | SSC   | 0.008  | 0.031  | -0.083  | -0.041  | 0.020   | -0.077  | -0.059  | 0.014   | 0.011  | 0.025  | 0.000  | 0.027  |
|                                                | SEN   | -0.049 | 0.501  | 0.273   | 0.471   | 0.363   | 0.436   | 0.523   | 0.650   | 0.683  | 0.951  | 0.911  | 0.896  |
|                                                | Hist. | 0.058  | 0.516  | 0.349   | 0.423   | 0.314   | 0.426   | 0.516   | 0.728   | 0.763  | 0.956  | 0.952  | 0.906  |
|                                                | TF    | 0.048  | 0.497  | 0.352   | 0.429   | 0.338   | 0.413   | 0.543   | 0.705   | 0.774  | 0.965  | 0.945  | 0.938  |
|                                                | TT    | 0.068  | 0.664  | 0.545   | 0.434   | 0.249   | 0.348   | 0.406   | 0.755   | 0.835  | 0.967  | 0.970  | 0.969  |
|                                                | TTM   | 0.043  | 0.490  | 0.466   | 0.408   | 0.170   | 0.429   | 0.494   | 0.702   | 0.708  | 0.949  | 0.948  | 0.924  |

TABLE 6.4 (CONT.) MONTHLY (SEASONAL) ANNUAL PARAMETERS FROM HISTORIC AND GENERATED SEQUENCES FOR NAN RIVER, (N.1)

| PARAMETER                | MODEL | APRIL   | MAY     | JUNE    | JULY     | AUG.     | SEPT.    | OCT.     | NOV.    | DEC.    | JAN.    | FEB.    | MARCH   |
|--------------------------|-------|---------|---------|---------|----------|----------|----------|----------|---------|---------|---------|---------|---------|
| Maximum                  | Hist. | 72.038  | 184.788 | 592.272 | 1404.420 | 1236.210 | 1647.389 | 569.430  | 221.700 | 102.490 | 70.243  | 50.283  | 44.880  |
|                          | TF    | 134.868 | 330.799 | 917.505 | 2684.296 | 1774.477 | 2727.116 | 1153.088 | 327.546 | 159.949 | 105.129 | 98.385  | 87.574  |
|                          | TT    | 277.021 | 413.921 | 828.891 | 2111.693 | 2202.762 | 3170.673 | 1282.946 | 496.270 | 335.004 | 209.685 | 171.249 | 141.382 |
|                          | TTM   | 134.024 | 321.276 | 738.640 | 1857.379 | 1597.922 | 1953.400 | 608.576  | 272.100 | 159.067 | 110.645 | 68.852  | 56.964  |
|                          | FM    | 114.473 | 464.000 | 852.172 | 1742.255 | 3467.244 | 2370.294 | 899.342  | 404.159 | 216.533 | 169.028 | 129.242 | 149.195 |
|                          | FMM   | 94.170  | 298.241 | 491.672 | 590.445  | 2299.444 | 1604.519 | 668.148  | 358.614 | 192.150 | 124.590 | 79.456  | 70.701  |
|                          | FSC   | 124.537 | 331.756 | 867.522 | 2642.268 | 2214.448 | 2785.287 | 1176.533 | 353.407 | 149.841 | 108.879 | 76.780  | 77.020  |
|                          | SSC   | 141.014 | 260.912 | 739.914 | 2380.762 | 1607.532 | 2238.812 | 1023.528 | 340.118 | 153.090 | 89.792  | 116.434 | 88.966  |
|                          | SEN   | 94.817  | 251.169 | 925.942 | 2313.049 | 1768.772 | 2611.972 | 938.654  | 329.165 | 171.295 | 118.547 | 101.424 | 101.708 |
|                          |       |         |         |         |          |          |          |          |         |         |         |         |         |
| Minimum                  | Hist. | 6.838   | 16.063  | 25.363  | 82.866   | 377.598  | 178.243  | 86.746   | 41.697  | 27.471  | 13.418  | 9.439   | 7.962   |
|                          | TF    | 0.000   | 0.000   | 0.000   | 19.659   | 0.000    | 0.000    | 31.459   | 13.831  | 0.000   | 0.000   | 0.000   | 0.000   |
|                          | TT    | 0.000   | 0.000   | 1.576   | 7.556    | 0.000    | 0.000    | 4.214    | 3.640   | 0.000   | 0.000   | 0.000   | 0.000   |
|                          | TTM   | 0.000   | 0.000   | 1.247   | 5.573    | 0.000    | 0.000    | 9.857    | 8.236   | 0.000   | 0.000   | 0.000   | 0.000   |
|                          | FM    | 0.190   | 0.697   | 3.263   | 11.884   | 29.366   | 16.129   | 4.209    | 2.137   | 1.070   | 0.729   | 0.399   | 0.286   |
|                          | FMM   | 1.090   | 3.340   | 1.717   | 16.538   | 25.557   | 21.058   | 8.140    | 4.614   | 2.485   | 1.373   | 0.840   | 0.721   |
|                          | FSC   | 0.000   | 0.000   | 0.000   | 2.163    | 0.000    | 0.000    | 30.690   | 13.682  | 0.000   | 0.000   | 0.795   | 1.107   |
|                          | SSC   | 0.000   | 0.000   | 58.735  | 0.000    | 0.000    | 0.000    | 0.000    | 2.972   | 0.000   | 0.000   | 0.000   | 0.000   |
|                          | SEN   | 0.000   | 0.000   | 1.048   | 0.000    | 0.000    | 0.000    | 21.906   | 27.686  | 0.867   | 0.000   | 0.000   | 0.000   |
|                          |       |         |         |         |          |          |          |          |         |         |         |         |         |
| Percentage of zero flows | Hist. | 0.000   | 0.000   | 0.000   | 0.000    | 0.000    | 0.000    | 0.000    | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   |
|                          | TF    | 2.600   | 2.300   | 0.100   | 0.000    | 0.100    | 2.600    | 0.000    | 0.000   | 0.400   | 0.700   | 0.900   | 0.900   |
|                          | TT    | 2.500   | 2.200   | 0.000   | 0.000    | 0.100    | 2.000    | 0.000    | 0.000   | 0.400   | 0.900   | 1.700   | 1.700   |
|                          | TTM   | 2.900   | 1.900   | 0.000   | 0.000    | 0.400    | 4.900    | 0.000    | 0.000   | 0.700   | 1.400   | 2.500   | 2.500   |
|                          | FM    | 0.000   | 0.000   | 0.000   | 0.000    | 0.000    | 0.000    | 0.000    | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   |
|                          | FMM   | 0.000   | 0.000   | 0.000   | 0.000    | 0.000    | 0.000    | 0.000    | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   |
|                          | FSC   | 0.000   | 0.000   | 0.600   | 0.000    | 0.200    | 0.000    | 0.000    | 0.000   | 0.200   | 0.500   | 0.000   | 0.000   |
|                          | SSC   | 4.300   | 1.200   | 0.000   | 0.300    | 0.100    | 3.000    | 0.200    | 0.000   | 0.400   | 1.500   | 0.800   | 1.500   |
|                          | SEN   | 2.400   | 1.700   | 0.000   | 0.500    | 0.300    | 3.200    | 0.000    | 0.000   | 0.000   | 0.100   | 0.400   | 0.600   |

TABLE 6.5 MONTHLY (SEASONAL) PARAMETERS FROM HISTORIC AND GENERATED SEQUENCES FOR NAM MAE TAENG, (P.4A)

| PARAMETER                                            | MODEL | APRIL  | MAY    | JUNE   | JULY   | AUG.    | SEPT.   | OCT.    | NOV.   | DEC.   | JAN.   | FEB.   | MARCH  |
|------------------------------------------------------|-------|--------|--------|--------|--------|---------|---------|---------|--------|--------|--------|--------|--------|
| Mean<br>$\times 10^6 \text{ cu. m}$                  | Hist. | 9.669  | 24.345 | 43.637 | 39.463 | 108.411 | 136.214 | 96.103  | 74.256 | 48.298 | 23.850 | 12.294 | 9.096  |
|                                                      | TF    | 11.588 | 26.513 | 44.028 | 38.429 | 104.632 | 133.838 | 92.917  | 71.132 | 48.346 | 23.614 | 15.114 | 13.302 |
|                                                      | TT    | 14.045 | 31.526 | 49.892 | 39.882 | 100.812 | 131.976 | 96.652  | 67.993 | 53.315 | 24.128 | 16.447 | 14.528 |
|                                                      | TTM   | 10.271 | 24.728 | 40.166 | 28.368 | 66.784  | 87.350  | 67.681  | 43.034 | 40.482 | 16.478 | 12.057 | 10.923 |
|                                                      | FM    | 10.075 | 27.700 | 47.454 | 41.983 | 106.467 | 141.199 | 98.722  | 71.530 | 51.885 | 22.772 | 12.333 | 9.274  |
|                                                      | FMM   | 8.410  | 34.340 | 66.378 | 30.441 | 88.384  | 125.753 | 106.557 | 89.834 | 66.135 | 14.274 | 6.033  | 4.856  |
|                                                      | FSC   | 9.946  | 24.538 | 43.518 | 38.563 | 105.541 | 133.543 | 93.466  | 72.592 | 48.613 | 22.991 | 12.280 | 9.386  |
|                                                      | SSC   | 9.618  | 23.454 | 43.120 | 40.522 | 101.685 | 136.156 | 95.170  | 68.192 | 47.589 | 21.093 | 22.178 | 7.678  |
|                                                      | SEN   | 10.669 | 23.370 | 44.630 | 39.808 | 105.023 | 131.090 | 92.825  | 70.003 | 48.360 | 23.037 | 14.582 | 10.689 |
|                                                      | SEN   | 10.603 | 14.825 | 23.897 | 27.378 | 100.273 | 103.517 | 60.288  | 66.772 | 22.624 | 23.625 | 11.559 | 8.513  |
| Standard<br>Deviation<br>$\times 10^6 \text{ cu. m}$ | Hist. | 10.371 | 13.750 | 24.394 | 26.046 | 94.740  | 93.949  | 53.210  | 58.612 | 21.761 | 23.617 | 11.328 | 7.972  |
|                                                      | TF    | 17.843 | 28.328 | 39.343 | 30.772 | 74.340  | 90.160  | 62.775  | 53.364 | 36.402 | 25.382 | 14.168 | 11.291 |
|                                                      | TT    | 8.118  | 11.818 | 20.889 | 21.436 | 51.747  | 44.753  | 29.288  | 30.920 | 16.397 | 15.859 | 8.131  | 5.773  |
|                                                      | TTM   | 11.532 | 20.397 | 35.578 | 36.687 | 79.047  | 88.161  | 61.219  | 56.189 | 31.054 | 17.796 | 11.929 | 9.293  |
|                                                      | FM    | 11.017 | 25.695 | 57.125 | 30.945 | 69.444  | 93.575  | 72.947  | 72.586 | 43.551 | 14.380 | 6.102  | 5.396  |
|                                                      | FMM   | 9.255  | 13.148 | 23.441 | 25.512 | 94.529  | 107.396 | 53.972  | 60.533 | 21.967 | 21.101 | 10.779 | 7.657  |
|                                                      | FSC   | 11.019 | 11.971 | 23.014 | 27.255 | 86.982  | 107.396 | 57.804  | 56.366 | 21.983 | 0.000  | 14.298 | 6.495  |
|                                                      | SSC   | 10.040 | 13.753 | 23.941 | 27.555 | 90.586  | 87.979  | 51.560  | 56.051 | 22.806 | 21.552 | 12.201 | 8.455  |
|                                                      | SEN   | 2.142  | 2.601  | 1.396  | 0.601  | 3.603   | 2.723   | 2.532   | 2.653  | 1.879  | 3.164  | 1.105  | 0.832  |
|                                                      | SEN   | 2.286  | 2.504  | 1.548  | 0.751  | 3.297   | 2.308   | 2.344   | 2.497  | 1.790  | 3.684  | 3.167  | 3.139  |
| Skewness                                             | TF    | 4.326  | 3.233  | 2.137  | 1.552  | 1.708   | 3.064   | 2.658   | 2.302  | 2.234  | 3.339  | 3.043  | 2.794  |
|                                                      | TT    | 2.249  | 2.801  | 1.583  | 1.023  | 1.856   | 2.060   | 2.074   | 2.025  | 1.876  | 2.196  | 2.566  | 2.458  |
|                                                      | TTM   | 2.280  | 1.942  | 2.360  | 2.272  | 3.260   | 1.852   | 2.104   | 2.938  | 1.704  | 1.820  | 1.972  | 1.990  |
|                                                      | FM    | 1.320  | 2.755  | 3.059  | 3.145  | 1.893   | 1.169   | 1.607   | 1.997  | 1.941  | 2.277  | 1.408  | 1.377  |
|                                                      | FMM   | 2.018  | 2.666  | 1.521  | 0.824  | 3.351   | 2.263   | 2.526   | 2.677  | 1.800  | 3.266  | 1.517  | 1.064  |
|                                                      | FSC   | 2.251  | 2.826  | 1.193  | 0.666  | 4.044   | 4.337   | 4.670   | 2.057  | 1.158  | 1.001  | 8.367  | 2.548  |
|                                                      | SSC   | 2.389  | 2.117  | 1.236  | 0.690  | 2.859   | 2.510   | 2.347   | 2.503  | 2.176  | 2.178  | 4.721  | 4.180  |
|                                                      | SEN   | 0.420  | 0.718  | 0.177  | 0.139  | 0.562   | 0.501   | 0.779   | 0.691  | 0.582  | 0.776  | 0.858  | 0.947  |
|                                                      | TF    | 0.380  | 0.742  | 0.142  | 0.120  | 0.611   | 0.520   | 0.825   | 0.679  | 0.545  | 0.754  | 0.883  | 0.993  |
|                                                      | TT    | 0.088  | 0.839  | 0.620  | 0.264  | 0.812   | 0.491   | 0.794   | 0.740  | 0.492  | 0.718  | 0.838  | 0.980  |
| Lag one<br>auto-<br>correlation<br>coefficient       | TTM   | 0.063  | 0.725  | 0.200  | 0.065  | 0.850   | 0.582   | 0.792   | 0.710  | 0.347  | 0.757  | 0.815  | 0.987  |
|                                                      | FM    | -0.008 | 0.506  | 0.713  | 0.291  | 0.560   | 0.503   | 0.684   | 0.600  | 0.613  | 0.469  | 0.858  | 0.964  |
|                                                      | FMM   | -0.023 | 0.572  | 0.894  | 0.580  | 0.260   | 0.120   | 0.448   | 0.455  | 0.919  | 0.445  | 0.530  | 0.934  |
|                                                      | FSC   | 0.603  | 0.564  | 0.538  | 0.572  | 0.606   | 0.624   | 0.638   | 0.564  | 0.571  | 0.663  | 0.554  | 0.556  |
|                                                      | SSC   | -0.008 | 0.007  | -0.067 | 0.016  | -0.006  | -0.082  | -0.008  | -0.019 | -0.009 | 0.000  | 0.000  | -0.023 |
|                                                      | SEN   | 0.641  | 0.757  | 0.139  | 0.224  | 0.622   | 0.499   | 0.772   | 0.694  | 0.456  | 0.877  | 0.736  | 0.950  |



TABLE 6.6 MONTHLY (SEASONAL) PARAMETERS FROM HISTORIC AND GENERATED SEQUENCES FOR NAM MAE CHAEM, (P.14)

| PARAMETER                                      | MODEL | APRIL  | MAY    | JUNE   | JULY   | AUG.    | SEPT.   | OCT.    | NOV.    | DEC.   | JAN.   | FEB.   | MARCH  |
|------------------------------------------------|-------|--------|--------|--------|--------|---------|---------|---------|---------|--------|--------|--------|--------|
| Mean<br>x 10 <sup>6</sup> cu.m                 | Hist. | 23.919 | 46.615 | 61.423 | 91.999 | 182.137 | 256.225 | 197.551 | 108.101 | 69.396 | 50.803 | 32.028 | 25.046 |
|                                                | TF    | 23.314 | 46.216 | 61.035 | 89.487 | 181.633 | 257.650 | 195.606 | 108.456 | 69.391 | 50.693 | 31.620 | 24.695 |
|                                                | TT    | 25.547 | 50.033 | 64.109 | 95.088 | 188.006 | 261.034 | 201.462 | 113.378 | 73.199 | 53.463 | 33.040 | 25.336 |
|                                                | TTM   | 21.844 | 44.242 | 54.895 | 77.733 | 151.467 | 197.442 | 155.808 | 92.916  | 61.113 | 44.529 | 26.893 | 19.946 |
|                                                | FM    | 23.782 | 49.040 | 65.004 | 96.317 | 190.257 | 265.718 | 199.623 | 110.904 | 71.464 | 52.335 | 32.336 | 24.914 |
|                                                | FMM   | 25.296 | 44.393 | 67.740 | 94.599 | 169.978 | 245.641 | 215.631 | 129.437 | 76.791 | 57.189 | 32.360 | 24.617 |
|                                                | FSC   | 23.241 | 45.837 | 60.711 | 89.231 | 180.919 | 256.651 | 194.146 | 107.947 | 70.139 | 50.964 | 31.722 | 24.261 |
|                                                | SSC   | 23.806 | 45.959 | 60.853 | 92.838 | 180.763 | 265.493 | 188.374 | 107.135 | 68.239 | 50.967 | 30.102 | 22.928 |
|                                                | SEN   | 23.298 | 47.105 | 62.360 | 92.465 | 179.950 | 253.634 | 191.846 | 106.155 | 68.510 | 49.781 | 31.348 | 24.557 |
|                                                | SEN   | 23.298 | 47.105 | 62.360 | 92.465 | 179.950 | 253.634 | 191.846 | 106.155 | 68.510 | 49.781 | 31.348 | 24.557 |
| Standard<br>Deviation<br>x10 <sup>6</sup> cu.m | Hist. | 14.647 | 21.863 | 25.966 | 44.289 | 75.868  | 112.738 | 90.663  | 39.347  | 22.985 | 18.559 | 14.589 | 14.248 |
|                                                | TF    | 12.821 | 21.614 | 26.449 | 42.290 | 75.400  | 114.312 | 84.042  | 37.973  | 21.620 | 17.309 | 12.876 | 12.253 |
|                                                | TT    | 17.791 | 29.827 | 32.176 | 46.056 | 77.313  | 112.211 | 84.530  | 48.295  | 29.822 | 22.618 | 15.251 | 13.372 |
|                                                | TTM   | 12.663 | 20.203 | 20.673 | 32.582 | 62.819  | 86.897  | 54.431  | 33.802  | 18.618 | 15.112 | 11.192 | 10.553 |
|                                                | FM    | 15.595 | 24.607 | 32.025 | 44.452 | 77.379  | 111.282 | 78.238  | 46.662  | 24.899 | 18.864 | 11.942 | 10.350 |
|                                                | FMM   | 11.580 | 20.441 | 34.033 | 45.240 | 58.917  | 105.183 | 71.848  | 45.013  | 26.273 | 18.212 | 9.511  | 9.379  |
|                                                | FSC   | 12.366 | 20.950 | 25.973 | 40.095 | 73.283  | 113.216 | 83.938  | 37.788  | 22.901 | 18.559 | 13.909 | 11.971 |
|                                                | SSC   | 15.345 | 21.881 | 24.710 | 45.662 | 76.293  | 112.957 | 71.889  | 38.796  | 20.219 | 16.183 | 0.000  | 0.000  |
|                                                | SEN   | 12.225 | 21.377 | 26.037 | 44.865 | 74.230  | 109.228 | 77.178  | 35.971  | 20.700 | 14.611 | 11.068 | 10.557 |
|                                                | SEN   | 12.225 | 21.377 | 26.037 | 44.865 | 74.230  | 109.228 | 77.178  | 35.971  | 20.700 | 14.611 | 11.068 | 10.557 |
| Skewness                                       | Hist. | 2.569  | 1.241  | 1.160  | 1.663  | 0.774   | 0.393   | 2.415   | 0.716   | 0.991  | 1.566  | 2.274  | 2.638  |
|                                                | TF    | 2.213  | 1.210  | 1.325  | 1.783  | 0.882   | 0.342   | 2.319   | 0.484   | 0.621  | 0.964  | 0.970  | 0.992  |
|                                                | TT    | 2.441  | 1.738  | 1.247  | 1.260  | 0.859   | 0.985   | 1.512   | 0.968   | 1.033  | 1.154  | 1.182  | 1.183  |
|                                                | TTM   | 2.982  | 1.307  | 0.967  | 1.573  | 0.864   | 0.635   | 1.364   | 0.335   | 0.465  | 0.882  | 0.887  | 0.945  |
|                                                | FM    | 2.526  | 1.486  | 1.320  | 1.410  | 1.118   | 1.262   | 1.054   | 1.391   | 0.925  | 1.018  | 1.370  | 1.801  |
|                                                | FMM   | 1.271  | 1.019  | 1.149  | 1.300  | 1.046   | 0.551   | 0.745   | 0.980   | 1.543  | 0.966  | 1.075  | 1.574  |
|                                                | FSC   | 2.302  | 1.095  | 1.193  | 1.617  | 0.765   | 0.308   | 2.053   | 0.363   | 0.846  | 1.937  | 2.376  | 2.083  |
|                                                | SSC   | 2.732  | 1.044  | 0.978  | 1.555  | 0.684   | 0.157   | 2.467   | 0.218   | 2.520  | 4.413  | 1.002  | 1.002  |
|                                                | SEN   | 1.510  | 1.142  | 1.017  | 1.620  | 0.760   | 0.343   | 2.347   | 0.707   | 1.274  | 1.276  | 2.703  | 2.436  |
|                                                | SEN   | 1.510  | 1.142  | 1.017  | 1.620  | 0.760   | 0.343   | 2.347   | 0.707   | 1.274  | 1.276  | 2.703  | 2.436  |
| Lag one<br>auto-<br>correlation<br>coefficient | Hist. | 0.583  | 0.330  | 0.384  | 0.408  | 0.572   | 0.520   | 0.502   | 0.621   | 0.875  | 0.941  | 0.947  | 0.977  |
|                                                | TF    | 0.590  | 0.456  | 0.367  | 0.417  | 0.580   | 0.530   | 0.588   | 0.557   | 0.908  | 0.957  | 1.000  | 1.000  |
|                                                | TT    | 0.381  | 0.649  | 0.617  | 0.524  | 0.572   | 0.446   | 0.559   | 0.598   | 0.933  | 0.974  | 0.990  | 0.987  |
|                                                | TTM   | 0.031  | 0.450  | 0.407  | 0.439  | 0.472   | 0.392   | 0.710   | 0.465   | 0.920  | 0.927  | 1.000  | 0.999  |
|                                                | FM    | 0.132  | 0.517  | 0.500  | 0.449  | 0.585   | 0.496   | 0.400   | 0.655   | 0.894  | 0.924  | 0.910  | 0.934  |
|                                                | FMM   | 0.236  | 0.369  | 0.809  | 0.708  | 0.704   | 0.504   | 0.512   | 0.610   | 0.906  | 0.845  | 0.887  | 0.913  |
|                                                | FSC   | 0.657  | 0.577  | 0.627  | 0.698  | 0.638   | 0.653   | 0.751   | 0.595   | 0.654  | 0.672  | 0.701  | 0.728  |
|                                                | SSC   | 0.000  | 0.027  | -0.084 | -0.001 | 0.052   | -0.049  | -0.037  | -0.007  | -0.001 | 0.041  | 0.000  | 1.000  |
|                                                | SEN   | 0.651  | 0.470  | 0.375  | 0.437  | 0.566   | 0.494   | 0.528   | 0.526   | 0.852  | 1.000  | 0.901  | 0.967  |
|                                                | SEN   | 0.651  | 0.470  | 0.375  | 0.437  | 0.566   | 0.494   | 0.528   | 0.526   | 0.852  | 1.000  | 0.901  | 0.967  |













TABLE 6.9(Cont.) MONTHLY (SEASONAL) PARAMETERS FROM HISTORIC AND GENERATED SEQUENCES FOR NGAO RIVER, (Y.13)

| PARAMETER                | MODEL | APRIL  | MAY    | JUNE   | JULY   | AUG.   | SEPT.   | OCT.   | NOV.   | DEC.   | JAN.   | FEB.   | MARCH  |
|--------------------------|-------|--------|--------|--------|--------|--------|---------|--------|--------|--------|--------|--------|--------|
| Maximum                  | Hist. | 5.827  | 21.064 | 18.936 | 35.385 | 60.001 | 69.379  | 35.770 | 32.144 | 12.027 | 12.813 | 6.238  | 5.879  |
|                          | TF    | 13.309 | 41.570 | 32.956 | 79.209 | 93.559 | 103.314 | 63.730 | 62.574 | 22.457 | 21.862 | 11.180 | 11.285 |
|                          | TT    | 23.481 | 38.868 | 43.940 | 48.017 | 69.353 | 113.379 | 95.767 | 49.479 | 21.703 | 19.653 | 11.823 | 11.800 |
|                          | TTM   | 10.786 | 38.454 | 25.258 | 51.469 | 63.626 | 64.674  | 43.208 | 34.862 | 12.217 | 11.339 | 5.593  | 5.598  |
|                          | FM    | 9.976  | 36.722 | 35.560 | 43.078 | 61.980 | 86.077  | 78.848 | 46.800 | 17.511 | 18.655 | 10.064 | 9.485  |
|                          | FMM   | 7.433  | 11.902 | 21.275 | 21.319 | 44.021 | 61.788  | 52.076 | 26.485 | 12.004 | 4.118  | 3.108  | 3.806  |
|                          | FSC   | 12.431 | 36.657 | 33.857 | 81.657 | 88.769 | 102.688 | 64.506 | 62.483 | 21.016 | 28.214 | 13.303 | 10.076 |
|                          | SSC   | 13.644 | 32.781 | 30.821 | 74.633 | 89.021 | 107.043 | 45.283 | 61.529 | 19.920 | 32.686 | 13.737 | 14.094 |
|                          | SEN   | 8.806  | 30.608 | 33.634 | 67.474 | 92.576 | 93.395  | 55.230 | 64.269 | 22.009 | 21.950 | 10.734 | 10.776 |
|                          | Hist. | 0.069  | 0.557  | 0.521  | 0.769  | 4.076  | 8.916   | 3.105  | 0.457  | 0.499  | 0.176  | 0.000  | 0.000  |
| Minimum                  | TF    | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 3.775   | 0.000  | 0.000  | 0.140  | 0.000  | 0.000  | 0.010  |
|                          | TT    | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000   | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  |
|                          | TTM   | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000   | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  |
|                          | FM    | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000   | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  |
|                          | FMM   | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000   | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  |
|                          | FSC   | 0.000  | 0.259  | 0.000  | 0.000  | 0.000  | 0.000   | 3.463  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  |
|                          | SSC   | 0.000  | 0.065  | 0.000  | 0.000  | 0.000  | 5.061   | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  |
|                          | SEN   | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000   | 0.000  | 0.460  | 0.209  | 0.000  | 0.000  | 0.000  |
|                          | Hist. | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000   | 0.000  | 0.000  | 0.000  | 0.000  | 4.000  | 4.000  |
|                          | TF    | 6.800  | 0.100  | 11.800 | 6.200  | 0.800  | 0.000   | 0.800  | 0.100  | 0.000  | 15.100 | 11.600 | 0.000  |
| Percentage of zero flows | TT    | 6.300  | 0.600  | 11.300 | 7.000  | 1.900  | 0.600   | 1.600  | 0.600  | 0.600  | 16.000 | 12.500 | 14.900 |
|                          | TTM   | 6.700  | 0.600  | 11.300 | 8.800  | 3.400  | 0.600   | 2.500  | 0.600  | 0.600  | 21.000 | 16.800 | 19.400 |
|                          | FM    | 0.600  | 0.600  | 0.600  | 0.600  | 0.600  | 0.600   | 0.600  | 0.600  | 0.600  | 0.600  | 3.700  | 3.700  |
|                          | FMM   | 0.600  | 0.600  | 0.600  | 0.600  | 0.600  | 0.600   | 0.600  | 0.600  | 0.600  | 0.600  | 10.600 | 10.600 |
|                          | FSC   | 0.000  | 0.000  | 9.800  | 0.000  | 0.000  | 0.000   | 0.000  | 0.000  | 0.700  | 8.800  | 0.000  | 11.000 |
|                          | SSC   | 11.300 | 0.000  | 12.300 | 8.800  | 2.800  | 0.000   | 1.700  | 4.000  | 1.500  | 1.100  | 2.300  | 2.200  |
|                          | SEN   | 5.900  | 0.600  | 10.400 | 7.500  | 2.300  | 0.100   | 0.600  | 0.000  | 0.000  | 12.400 | 9.700  | 12.100 |
|                          | Hist. | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000   | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  |
|                          | TF    | 6.800  | 0.100  | 11.800 | 6.200  | 0.800  | 0.000   | 0.800  | 0.100  | 0.000  | 15.100 | 11.600 | 0.000  |
|                          | TT    | 6.300  | 0.600  | 11.300 | 7.000  | 1.900  | 0.600   | 1.600  | 0.600  | 0.600  | 16.000 | 12.500 | 14.900 |



