

CHAPTER 4

Kinetic Studies by Dilatometry

The kinetics of the bulk ring-opening polymerisation of ϵ -caprolactone using tin(II) alkoxides were studied in detail using dilatometry as the analytical technique for following the progress of the reaction. Because the polymerisation of a liquid monomer is generally accompanied by a decrease in volume, dilatometry utilizes the volume change that occurs upon polymerisation to follow conversion versus time. Therefore, dilatometry is only a convenient but indirect way to record the progress of monomer conversion. This method has been widely used for kinetic studies in polymer science since the equipment is relatively simple and inexpensive.

In this experiment, the rate of polymerisation will be measured by the dilatometer developed as described in section 4.3. The dilatometer is placed in a constant temperature bath and the volume change in the capillary of the polymerising system, which is quantitatively related to the percent conversion, is followed with time. Dilatometry is not useful for most step polymerisations where there is a small molecule by-product and which results in no appreciable volume change upon polymerisation.

4.1 Homopolymer Polymerisation

4.1.1 Monomer

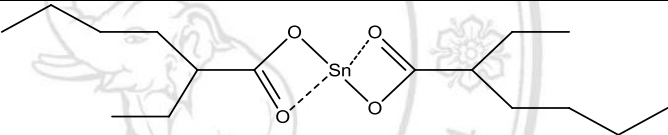
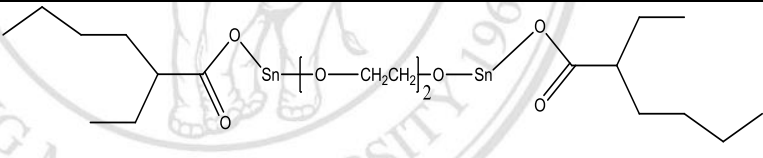
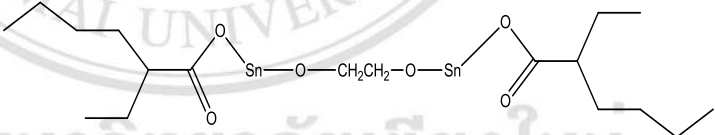
ϵ -Caprolactone (ϵ -CL) is chosen for the kinetic studies of its polymerisation with the synthesised novel initiators due to its easy polymerisability. Most importantly, its polymer (poly(ϵ -caprolactone), PCL) is also liquid at the polymerisation temperature used (130 °C). This made it amenable to dilatometry study in bulk since there was avoidance of the complication of verification or solidification occurring during the course of the experiments. Moreover, PCL is becoming increasingly important commercially, especially in certain biomedical applications because of its

biocompatibility and biodegradability and for polymer blends owing to its compatibility with a large range of polymers.

4.1.2 Initiators

The initiators used for these studies are the series of synthesised tin(II) alkoxides which are described in the chapter 3. Elementary work results showed that the solid initiators were hardly soluble in the monomer, while the liquid initiators were readily soluble. Therefore, the initiators used for kinetic studies by dilatometry were bis(tin(II) octoate) diethylene glycol ($[\text{Sn}(\text{Oct})_2\text{DEG}]$), bis(tin(II) octoate) ethylene glycol ($[\text{Sn}(\text{Oct})_2\text{EG}]$), and also commercially available tin(II) octoate and tin(II) octoate / HOROH mixtures. Their molecular formulae are shown in Table 4.1.

Table 4.1 The molecular formulae of initiators used for kinetic studies by dilatometry.

Initiator	Molecular formula
Tin(II) Octoate $\text{Sn}(\text{Oct})_2$	
Bis(tin(II) octoate) diethylene glycol $[\text{Sn}(\text{Oct})_2\text{DEG}]$	
Bis(tin(II) octoate) ethylene glycol $[\text{Sn}(\text{Oct})_2\text{EG}]$	

4.2 Design of Kinetic Experiments

For the kinetic investigations of polymerisations, a variety of methods and apparatus has been developed [43, 105-107]. In this work, the technique used for kinetic studies of the ROP of $\epsilon\text{-CL}$ is dilatometry. The dilatometric method is especially useful on account of its simplicity and general application which provide complementary information about the progress of a polymerisation reaction in terms of % conversion and rate of polymerisation.

The design and construction of small glass dilatometers depend on a number of considerations as mentioned before, such as the expected volume change and the accuracy with which it must be measured, the rate of polymerisation, the corresponding rate of heat evolution and its effect on temperature uniformity, the viscosity of the polymerising mixture, and the need for stirring. If, as is usual, a capillary is used to display the volume change, good temperature control throughout is essential, if possible to within ± 0.1 °C.

Dilatometry Apparatus

In this work, the dilatometer was designed and constructed as shown in Figure 4.1. It consisted of a round-bottomed flask with a quickfit neck into which a capillary column was inserted. The top of the capillary column was connected to a CaCl₂ drying tube to prevent the ingress of atmospheric moisture into the system. A small magnetic bar (1 cm) was placed inside the round-bottomed flask for the dual purpose of stirring the reaction mixture to maintain homogeneity and maximizing the efficiency of heat transfer to ensure good temperature control.

The dilatometer is placed in a thermostatically controlled oil bath maintained at the desired reaction temperature. As the polymerisation proceeds, liquid sample meniscus movement in the capillary is due to two factors:

- 1) Thermal expansion of the liquid sample.
- 2) Contraction due to polymerisation.

Initially, as the volume of liquid increases by thermal expansion, the liquid will rise up the capillary tube. As soon as the liquid has reached thermal equilibrium, the volume of the liquid will decrease with polymerisation. The change in height of the liquid in the capillary is measured periodically with a cathetometer. The rate of polymerisation can then be determined from the rate of change in the height of the liquid.

Good temperature control was achievable to within an acceptable ± 0.2 °C. Cathetometer readings of the meniscus height in the capillary were accurate to ± 0.001 cm.

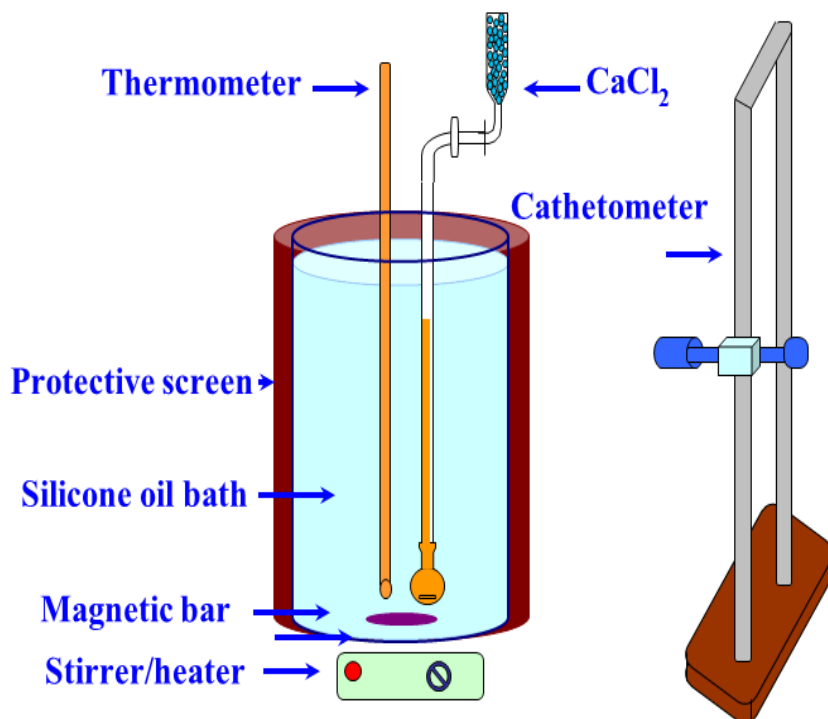


Figure 4.1 Dilatometry set-up used in kinetic studies of ROP of ϵ -CL.

4.3 Limitations of Dilatometry

It was shown that applications of this conventional dilatometer to bulk polymerisation reactions are limited by the following sources of error: a measurement of volume change is complicated if there are any gases dissolved in monomer which may be isolated as bubbles while the polymerisation occurs. The dilatometry technique will not be able to measure the volume contraction of a solid monomer: a problem of solvent evaporation at the polymerisation temperature could happen if the solid monomer is dissolved in a solvent. Since the monomer itself is used as a recording liquid for the volume decrease, its increasing viscosity soon causes a distortion of the meniscus in the capillary, resulting in a difficulty in reading. In addition, the dissipation of the heat of reaction by either convection or conduction is increasingly hindered by the increasing viscosity of the polymerising monomer/polymer mixture. A long period of thermal equilibration can occur as a result of using either too low an initiator concentration or too low a polymerisation temperature. Finally, when a high reactivity initiator or

initiator concentration is used, measurement of the meniscus height can be difficult since the polymerisation rate under this condition is fast.

4.4 Dilatometric Data Analysis

In a dilatometry experiment, after reaching thermal equilibrium, as the polymerisation proceeds the volume of the polymerising mixture decreases. The data of volume change that occurs upon polymerisation are then used to follow conversion versus time. The change in volume of the system, ΔV , may be related to the monomer concentration, reaction yield, and the rate of polymerisation as follows. The total volume of the system, V , at any time t is given by

$$V = W_m \bar{V}_m + W_p \bar{V}_p + W_s \bar{V}_s \quad (4.1)$$

where W_m , W_p and W_s are the weights and \bar{V}_m , \bar{V}_p and \bar{V}_s are the partial specific volumes of monomer, polymer and solvent (if used) respectively. To a very good approximation, $W_p = W_m^0 - W_m$, where W_m^0 is the initial weight of monomer. Combining this approximation and rearranging gives the weight of monomer at time t as

$$W_m = \frac{V - W_m^0 \bar{V}_p - W_s \bar{V}_s}{\bar{V}_m - \bar{V}_p} \quad (4.2)$$

Because no polymer is present initially, the initial volume V_0 is given by'

$$V_0 = W_m^0 \bar{V}_m + W_s \bar{V}_s \quad (4.3)$$

and, provided that all of the monomer is converted to polymer at the completion of the reaction, the final volume V_∞ is

$$V_\infty = W_m^0 \bar{V}_p + W_s \bar{V}_s \quad (4.4)$$

Of course, this assumption of complete (100 %) monomer conversion can only be an approximation since it is a thermodynamic fact that there will inevitably be a certain "equilibrium monomer concentration", $[M]_{eq}$, remaining in the reaction mixture at the final (constant) volume V_∞ . However, for ϵ -caprolactone bulk polymerisation over the

temperature range of 110-140 °C, this is believed to be a good approximation since the $[M]_{eq}$ for ϵ -caprolactone bulk polymerisation, as observed experimentally at 100 °C, has been reported to be very small (≈ 0) [108].

On the strength of this approximation, equations 4.3 and 4.4 may now be used to eliminate $\bar{V}_m - \bar{V}_p$ and $W_s \bar{V}_s$ from equation 4.2 and, when this is done, equation 4.5 is obtained.

$$W_m = \frac{V - V_\infty}{V_0 - V_\infty} W_m^o \quad (4.5)$$

The % conversion to polymer (or yield of the reaction) on a weight % basis, Y, may then be written as

$$\% \text{ Conversion} = Y = 100 \frac{W_m^o - W_m}{W_m^o} = 100 \frac{V_0 - V}{V_0 - V_\infty} \quad (4.6)$$

By using the dilatometry apparatus shown in Figure 4.1, change in volume, ΔV , is proportional to change in height of the liquid meniscus, Δh , in the capillary, as given by

$$\Delta V = V_0 - V = \pi r^2 \Delta h \quad (4.7)$$

where V_0 is the initial volume of the system, V is the volume at time t , and r is the capillary radius. Therefore equation 4.6 can be written as

$$\% \text{ Conversion} = Y = 100 \frac{\Delta V}{V_0 - V_\infty} = 100 \frac{\Delta h(t)}{\Delta h(\infty)} \quad (4.8)$$

where $\Delta h(t) = h_0 - h =$ progressive change in meniscus height at any time t

$\Delta h(\infty) = h_0 - h_\infty =$ final change in meniscus height at time ∞ (i.e., at constant h)

This % conversion in equation 4.8 is obviously a cumulative parameter, meaning that it is the total % conversion of monomer to polymer over the time period from the start of the polymerisation at time $t=0$ to any subsequent time t . Thus, the % conversion increases progressively from 0 % at the start to 100 % at the end.

Similarly, it is possible to proceed from equation 4.5 and utilize the definition of the rate of polymerisation, R_p , in equation 4.9.

$$R_p = \frac{-d[M]}{dt} = \lim_{\Delta t \rightarrow 0} \frac{\Delta[M]}{\Delta t} \quad (4.9)$$

However, the rate of polymerisation, R_p , in equation 4.9 is not a cumulative parameter. Instead, it can either be calculated as an **average** value over a long time period (usually starting from $t=0$) or as an **instantaneous** value over a very short (incremental) time period. Of these two, the instantaneous R_p is generally considered to be the more meaningful since it is an absolute value at a specific time rather than an average value over an ever-increasing time interval. Thus, combining this concept with the equation for the % conversion in equation 4.8 gives the instantaneous rate expression in equation 4.10.

$$R_p = \frac{\Delta Y [M]_0}{100 \Delta t} = \frac{\Delta h [M]_0}{\Delta h(\infty) \Delta t} \quad (4.10)$$

where Δh = incremental height change during Δt

$\Delta h(\infty) = h_0 - h_\infty$ = final change in meniscus height at time ∞ (i.e., at constant h)

Δt = incremental time interval between successive readings (mins)

$[M]_0$ = initial monomer concentration (mol l^{-1})

If two successive meniscus height readings h_1 and h_2 , taken at times t_1 and t_2 , gave % conversions of Y_1 and Y_2 from equation 4.8, then the value of R_p from equation 4.10 would be

$$R_p = \frac{\Delta Y [M]_0}{100 \Delta t} = \frac{Y_2 - Y_1 [M]_0}{100 (t_2 - t_1)} \quad (4.11)$$

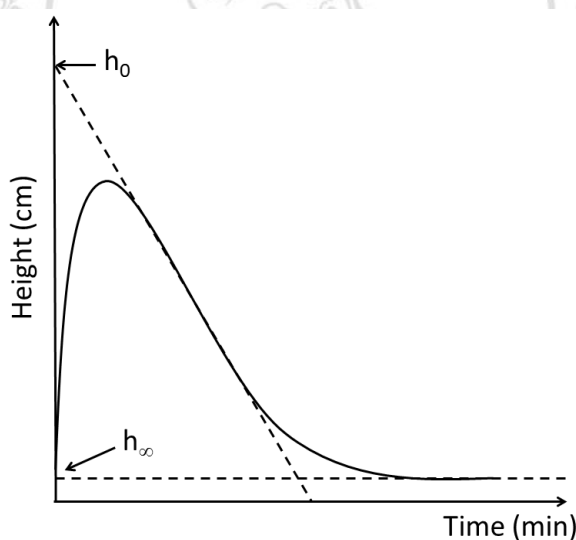
This R_p is an “average” value over the time interval $t_1 \rightarrow t_2$ but, because this time interval is very small (i.e., incremental) compared to the total time $t_0 \rightarrow t_\infty$ for the polymerisation as a whole, it can be regarded to a good approximation as an **instantaneous** R_p at (as an average) the mid-point of the time interval, i.e.

$$R_p \text{ at time } = \frac{t_1 + t_2}{2} \quad (4.12)$$

4.4.1 Initial Meniscus Height (h_0)

The true value of h_0 , the initial meniscus height, cannot be measured directly since, when the dilatometer is first placed in the heating bath, there is a thermal equilibrium period during which the dilatometer and its contents increase in temperature up to the bath temperature. This equilibrium period may be take several minutes. During this period, the meniscus height h increase due to thermal expansion. However, this increase soon changes to be a decrease as the dilatometer approaches the bath temperature and contraction due to the onset of polymerisation takes over.

Thus, the value of h_0 need to be estimated from the initial part of the raw data curve as carefully and as accurately as possible. This is usually done by waiting for the thermal equilibration period to be complete and then extrapolating the subsequent data points back to zero time ($t = 0$) as shown below.



4.4.2 Kinetic Analysis

4.4.2.1. First-Order Kinetics Analysis

It has been widely reported in the research literature that the bulk polymerisation of ϵ -caprolactone using coordination-insertion-type initiating systems is kinetically first-order ($n=1$) with respect to monomer, i.e.

$$\frac{-d[M]}{dt} = k_1[M] \quad (4.13)$$

which, when integrated between the limits of $[M]_0$ at time $t=0$ and $[M]_t$ at time $t=t$, gives the first-order rate equation of:

$$\ln([M]_0/[M]_t) = k_1 t \quad (4.14)$$

where k_1 is the first-order rate constant.

Given the correspondence from dilatometry (Infinite Time Method) that

$$\ln([M]_0/[M]_t) = \ln[(h_0 - h_\infty)/(h - h_\infty)] \quad (4.15)$$

the first-order rate equation can be expressed in terms of the primary dilatometric data (h, t) as

$$\ln[(h_0 - h_\infty)/(h - h_\infty)] = k_1 t \quad (4.16)$$

Therefore, for a first-order reaction, a semi-log plot of $\ln[(h_0 - h_\infty)/(h - h_\infty)]$ or $\ln([M]_0/[M]_t)$ against time t should yield a straight line graph of slope $= k_1 =$ the first order rate constant.

However, this rather simplified approach fails to take into account the well known reversibility of ring-opening polymerisations and the thermodynamic nature of the equilibrium. In a reversible ring-opening polymerisation, the propagation-depropagation equilibrium can be expressed as



where

- M = monomer
- M_n^* and M_{n+1}^* = propagation species
- k_p = rate constant for propagation
- k_{dp} = rate constant for depropagation

Therefore, the rate of propagation (polymerisation), R_p , is given by

$$R_p = -\frac{d[M]}{dt} = k_p[M_n^*][M] - k_{dp}[M_{n+1}^*] \quad (4.18)$$

At equilibrium, $R_p = 0$ and the remaining monomer concentration is what is known as the equilibrium monomer concentration $[M]_e$. It also can be assumed that $[M_n^*] = [M_{n+1}^*] = [M^*]$ (for any value of n). Thus, equation 4.18 becomes

$$\begin{aligned} k_p[M^*][M]_e &= k_{dp}[M^*] \\ k_p[M]_e &= k_{dp} \end{aligned} \quad (4.19)$$

$$[M]_e = \frac{k_{dp}}{k_p} \quad (4.20)$$

Combining eqs. (4.18) and (4.19) gives

$$\begin{aligned} -\frac{d[M]}{dt} &= k_p[M^*][M] - k_p[M]_e[M^*] \\ -\frac{d[M]}{dt} &= k_p[M^*]([M] - [M]_e) \end{aligned} \quad (4.21)$$

Integrating this rate equation 4.21 between the limits

initial monomer concentration = $[M]_0$ at time $t = 0$

intermediate monomer concentration = $[M]$ at any time t gives

$$-\int_{[M]_0}^{[M]} \frac{d[M]}{[M^*]([M] - [M]_e)} = \int_0^t k_p dt$$

where, according to the Steady-State Approximation

$[M^*] =$ propagating (active) species concentration

$=$ constant and therefore

$$\ln\left(\frac{[M]_0 - [M]_e}{[M] - [M]_e}\right) = k_p[M^*]t \quad (4.22)$$

Hence, if this rate equation is obeyed, a semi-log of

$$\ln\left(\frac{[M]_0 - [M]_e}{[M] - [M]_e}\right) \quad \text{against} \quad t$$

should give a straight line of slope = $k_p[M^*]$

The equilibrium monomer concentration, $[M]_e$, can either be obtained experimentally or theoretically. In this chapter, $[M]_e$ was determined experimentally as described below.

Experimental determination of $[M]_e$ is considered as a preferred method because it is based on real experimental data. At the end of each polymerisation reaction, the polymer yield was determined as *quantitatively* as possible by dissolution and precipitation followed by careful filtering and drying under vacuum to constant weight. Below is an example for ϵ -caprolactone polymerisation at 130 °C using 0.1 mol % mixture initiator ($\text{Sn}(\text{Oct})_2 / \text{EG}$) as initiator.

$$\begin{aligned} \text{\% yield of polymer} &= \left(\frac{\text{weight of the polymer obtained}}{\text{weight of the initial monomer}} \right) \times 100 \% \\ &= 99.71 \% \end{aligned}$$

$$\text{\% monomer remaining (at equilibrium)} = 0.29 \%$$

$$f = 0.0029$$

where f is the fraction of monomer remaining at equilibrium, i.e.

$$[M]_e = f [M]_0 \quad (4.23)$$

Combining Equations 4.22 and 4.23, then the rate equation is modified as follows.

$$\ln \left(\frac{[M]_0 - f [M]_0}{[M] - f [M]_0} \right) = k_p [M^*] t \quad (4.24)$$

When the kinetics of polymerisation is studied by dilatometry, the rate equation needs to be expressed in dilatometric terms.

$$\ln \left(\frac{(h_0 - h_\infty) - f (h_0 - h_\infty)}{(h - h_\infty) - f (h_0 - h_\infty)} \right) = k_p [M^*] t \quad (4.25)$$

or

$$\ln\left(\frac{(1-f)(h_0 - h_\infty)}{(h - h_\infty) - f(h_0 - h_\infty)}\right) = k_p[M^*]t \quad (4.26)$$

Where $[M]_0 \propto h_0 - h_\alpha$

$[M] \propto h - h_\alpha$

slope of linear part of the rate plot = $k_p[M^*] = k_{app}$

where k_{app} is the apparent first-order rate constant.

4.4.2.2. Zero-Order Kinetics Analysis

It is noticeable from the earlier % conversion-time profiles that they all have linear or near-linear portions from about 30 % conversion onwards. The % conversion-time plots are essentially zero-order kinetic plots. While this is not meant to imply that the polymerisation reaction is a zero-order reaction, it is possible that the opposing rate effects of decreasing monomer concentration and increasing initiator solubilisation could approximately balance each other resulting in pseudo-zero-order kinetics.

The zero-order rate equation is given by

$$-\frac{d[M]}{dt} = k_0$$

which when integrated gives

$$[M]_0 - [M]_t = k_0 t$$

where k_0 is the zero-order rate constant.

This equation can be alternatively expressed as:

$$p = k_0 t / [M]_0 \quad (4.27)$$

where $[M]_0$ = initial monomer concentration (mol l^{-1}) at time $t = 0$

$[M]_t$ = remaining monomer concentration (mol l^{-1}) at time t

k_0 = zero-order rate constant ($\text{mol l}^{-1} \text{min}^{-1}$)

p = extent of reaction (or fraction of conversion)

Given that $p = ([M]_0 - [M]_t) / [M]_0 = (h_0 - h)/(h_0 - h_\infty)$ from dilatometry

A zero-order plot of p against time t should yield a (partial) straight line graph of slope $= k_0/[M]_0$. Knowing $[M]_0$, the value of k_0 , the zero-order rate constant, can be calculated.

4.4.3 Preliminary Experimental Results

Dilatometry experiments for kinetic analysis were carried out initially by setting the temperature of the silicone oil bath at the desired reaction temperature. The dilatometer, filled with a sample mixture of ϵ -caprolactone and the chosen initiator and set as described in section 4.3.1, was then placed in a thermostatically controlled oil bath maintained at 130 °C. Upon immersion of the dilatometer, the temperature of the oil bath quickly dropped by up to 7 °C before gradually increasing back up to 130 °C over a period of about 10 minutes. This led to an initial period of non-isothermal thermal equilibration during which the meniscus movement in the capillary was due to both thermal expansion of the liquid sample and contraction due to polymerisation. Data taken during this equilibration period was used to estimate the meniscus height at zero time (h_0) as described in the following section.

One way of shortening the thermal equilibration period was to start at a slightly higher temperature of 140 °C. Immediately after immersing the dilatometer in the oil bath, the temperature was re-set to 130 °C, whereupon the oil bath temperature dropped to about 127 °C, only 3 °C below the required temperature. In this way, thermal equilibration was shortened by a half and the experimental data gave a smoother curve, as shown for example in Figure 4.2. Consequently, this technique was used in all kinetic experiments in order to shorten the thermal equilibration time and thus provide more valid data points during the initial period.

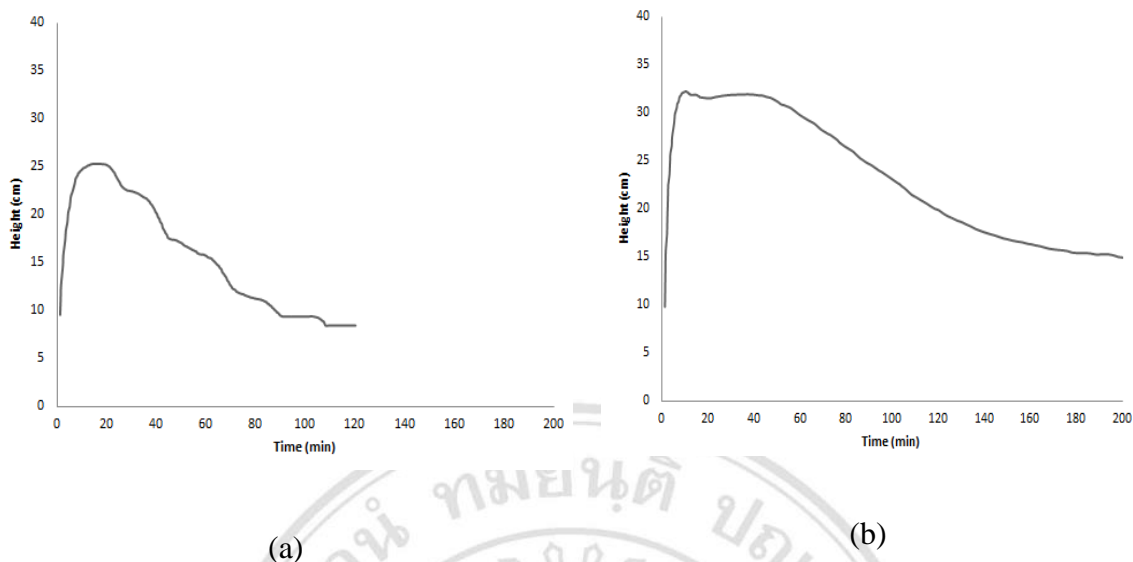


Figure 4.2 Dilatometric data for ϵ -caprolactone polymerisation at 130 °C using 0.10 mol % $\text{Sn}(\text{Oct})_2$; initial oil bath temperature set at (a) 130 °C and (b) 140 °C .

The data for all of the kinetic experiments are listed in Tables 4.3-4.7. These tables show the raw data values of meniscus height, h , at time, t , and the calculated values of % conversion using Equation 4.8. To calculate % conversion using Equation 4.8, h_0 and h_∞ needed to be determined as described in section 4.5.1. Figure 4.3 shows as an example how to determine h_0 and h_∞ for ϵ -caprolactone polymerisation using 0.1 mol % $\text{Sn}(\text{Oct})_2$ / EG as initiator at 130 °C. The kinetic profile of % conversion against time calculated from data in Figure 4.3 is shown in Figure 4.4.

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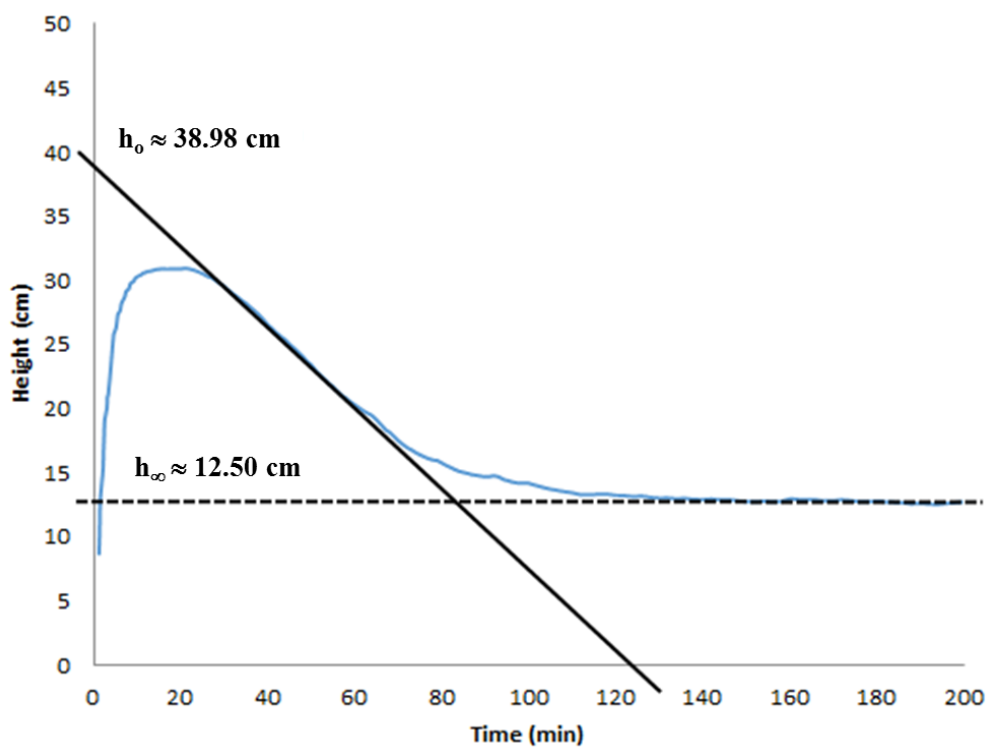


Figure 4.3 Extrapolation of h to zero time (h_0 at $t = 0$) and at constant height (h_∞) for ϵ -caprolactone polymerisation using 0.1 mol % $\text{Sn}(\text{Oct})_2 / \text{EG}$ as initiator at 130°C .

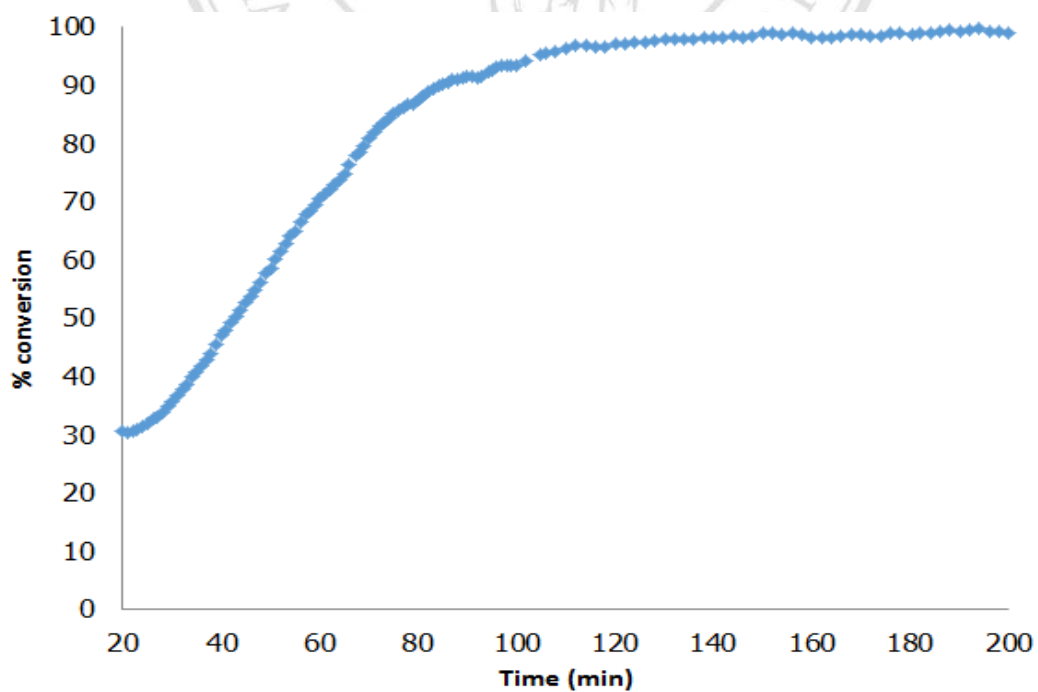


Figure 4.4 Kinetic profile of % conversion against time for ϵ -caprolactone using 0.1 mol % $\text{Sn}(\text{Oct})_2 / \text{EG}$ as initiator at 130°C .

First-Order and Zero-Order Rate Plots and Rate Constants

For most polymerisation reactions, a steady-state is usually reached within the first 20 % conversion. This steady-state then continues for the major part of the reaction (i.e. monomer conversion) until the monomer concentration becomes seriously depleted and/or the increase in viscosity of the system (especially in bulk) leads to diffusion-controlled processes becoming influential. Usually this occurs not later than about 80 % conversion. However, these limits (20-80 %) can vary markedly from system to system and so each kinetic plot needs to be considered individually. In this work, conversion limit was also chosen in the range of 20-80 % for constructing a first-order rate plot according to equation 4.26 as shown in Figure 4.5. The apparent first-order rate constant, k_{app} , could then be determined from the slope of this rate plot.

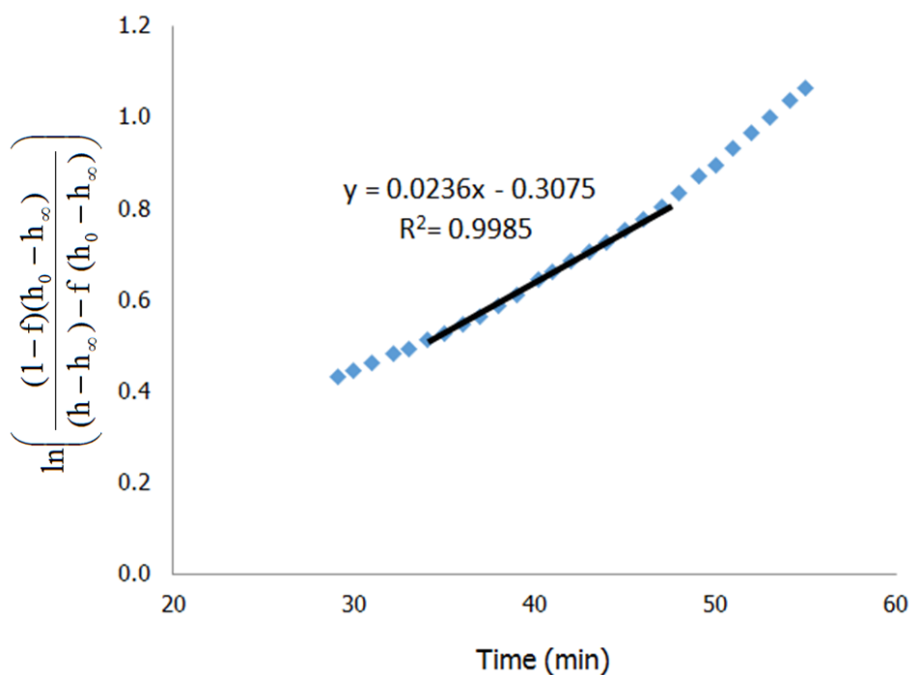


Figure 4.5 First-order rate plot from dilatometry for ϵ -caprolactone using 0.1 mol % $\text{Sn}(\text{Oct})_2 / \text{EG}$ as initiator at 130 °C.

Figure 4.6 shows a zero-order plot in the same range (20-80 % conversion) according to equation 4.27. From the slope ($= k_0 / [M]_0$) of this linear portion, the zero-order rate constants, k_0 , can be calculated, if $[M]_0$ is known.

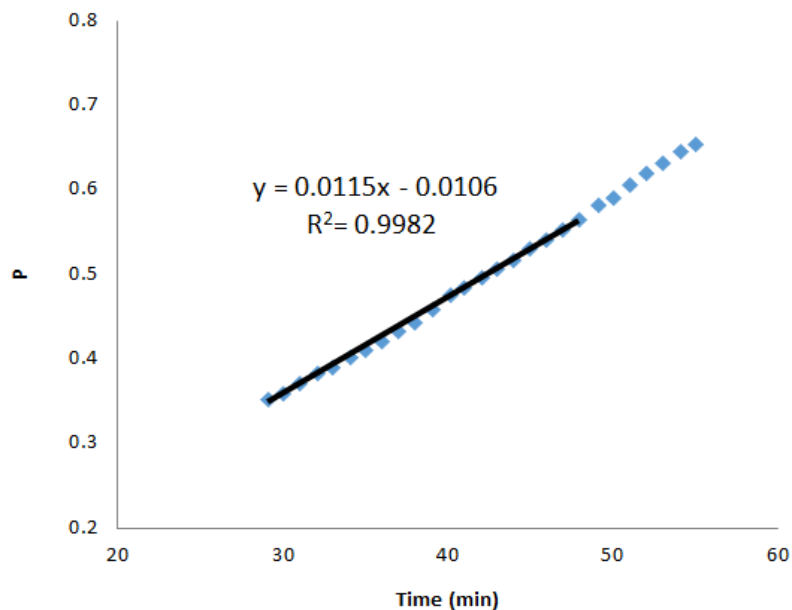


Figure 4.6 Zero-order rate plot from dilatometry for ϵ -caprolactone using 0.1 mol % $\text{Sn}(\text{Oct})_2 / \text{EG}$ as initiator at 130 °C.

Evaluation of $[\text{M}]_0$

The value of $[\text{M}]_0$, the initial molar concentration of the pure ϵ -caprolactone, at the polymerisation temperature (130 °C) is given by:

$$[\text{M}]_0 = \frac{\text{Density of caprolactone at 130 } ^\circ\text{C}}{\text{Molecular weight of } \epsilon\text{-caprolactone}}$$

Densities of ϵ -caprolactone monomer at various temperatures are listed in Table 4.2 and Figure 4.7 [4]. From the extrapolated values in this Figure, density of ϵ -caprolactone at 130 °C is found to be 0.996 g /cm³. Therefore, $[\text{M}]_0$ is calculated as below.

$$\begin{aligned} [\text{M}]_0 &= \frac{0.996 \text{ (g /cm}^3\text{)} \times 1000 \text{ (cm}^3 \text{/l)}}{114.15 \text{ (g / mol)}} \\ &= 8.725 \text{ mol /l} \end{aligned}$$

Table 4.2 Densities of ϵ -caprolactone monomer at various temperatures. [4]

Temperature (°C)	Monomer Density ρ_m (g / cm ³)
Experimental Values	
40	1.0485
50	1.0427
60	1.0351
70	1.0309
Extrapolated Values	
90	1.018
120	1.002
130	0.996
140	0.990

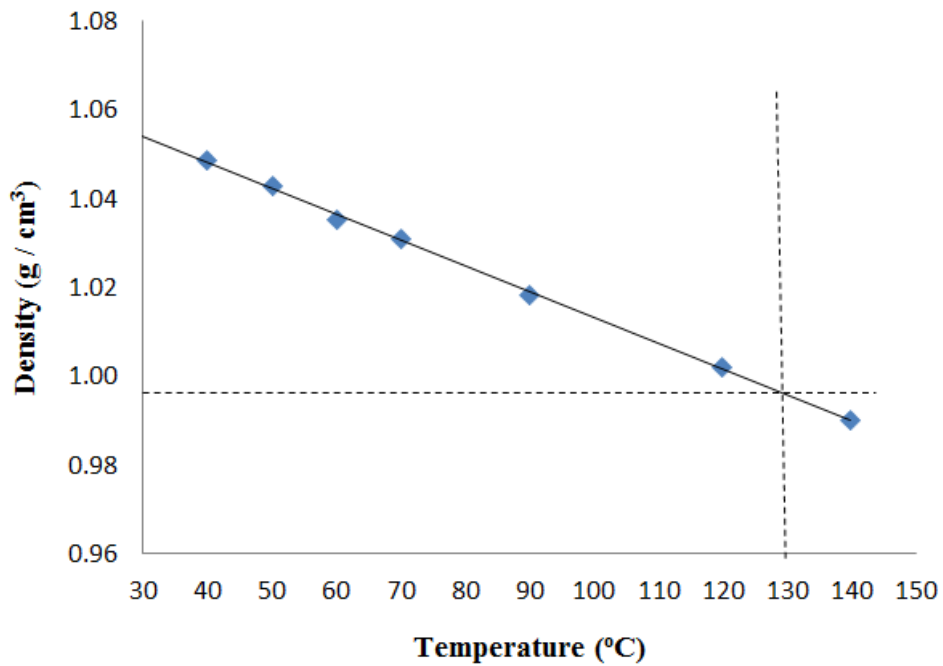


Figure 4.7 The linear decrease in density as a function of temperature for ϵ -caprolactone monomer.

4.4.4 Dilatometry Results

All raw data plots from the dilatometry experiments, kinetic profiles of % conversion against time, first-order rate plots and zero-order rate plots for ϵ -caprolactone using different initiator systems at 130 °C are shown in Figures 4.8-4.27.

Table 4.8 shows kinetic analysis results for all the dilatometry experiments explained above.



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Table 4.3 Dilatometry data of ϵ -caprolactone polymerisation at 130 °C using 0.1 mol % Sn(Oct)₂ as initiator.

Weight of ϵ -caprolactone = 14.6140 g h_0 (from extrapolation) = 39.98 cm

Weight of Sn(Oct)₂ = 0.0516 g % Yield = 96.39

Capillary diameter = 0.180 cm Residual monomer (f) = 0.036

Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion
1.13	9.800		8.15	31.870		20.00	31.520	32.45
1.25	11.750		8.30	31.950		21.00	31.520	32.45
1.40	14.175		8.41	32.015	Thermal	22.30	31.600	32.14
1.51	15.720		9.17	32.130	Equilibration	23.00	31.640	31.99
2.05	17.370		10.01	32.220		24.00	31.690	31.80
2.19	18.930		10.27	32.250	29.65	25.00	31.720	31.68
2.36	20.500		10.40	32.220	29.76	26.00	31.770	31.49
2.46	21.340		10.56	32.185	29.90	27.00	31.800	31.38
2.58	22.500		11.14	32.120	30.15	28.11	31.835	31.24
3.14	23.580		11.30	32.090	30.26	29.00	31.835	31.24
3.30	24.550		11.48	32.000	30.61	30.00	31.880	31.07
3.41	25.150	Thermal	12.00	31.950	30.80	31.00	31.880	31.07
3.51	25.770	Equilibration	12.30	31.875	31.09	32.00	31.880	31.07
4.08	26.550		13.00	31.860	31.15	33.00	31.920	30.92
4.18	26.975		13.30	31.860	31.15	34.00	31.910	30.95
4.33	27.575		14.00	31.890	31.03	35.00	31.910	30.95
5.11	28.860		14.30	31.890	31.03	36.00	31.910	30.95
5.34	29.525		15.00	31.860	31.15	37.00	31.950	30.80
5.53	29.925		15.30	31.790	31.41	38.00	31.910	30.95
6.24	30.500		16.00	31.715	31.70	39.00	31.910	30.95
6.39	30.720		16.30	31.625	32.05	40.00	31.885	31.05
6.52	30.940		17.00	31.600	32.14	41.00	31.850	31.18
7.06	31.170		17.30	31.580	32.22	42.00	31.820	31.30
7.21	31.350		18.00	31.570	32.26	43.00	31.815	31.32
7.37	31.520		18.30	31.540	32.37	44.00	31.770	31.49
7.55	31.700		19.00	31.540	32.37	45.00	31.680	31.84
8.05	31.800		19.30	31.525	32.43	46.00	31.615	32.09

Table 4.3 (Continued).

Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion
47.00	31.570	32.26	84.00	25.690	54.81	144.00	17.260	87.15
49.00	31.315	33.24	85.00	25.470	55.65	146.00	17.100	87.76
50.00	31.175	33.77	86.00	25.250	56.50	148.00	16.930	88.41
51.00	30.990	34.48	87.00	25.100	57.07	150.00	16.825	88.81
51.30	30.920	34.75	88.00	24.920	57.76	152.00	16.700	89.29
52.00	30.850	35.02	89.00	24.770	58.34	154.00	16.600	89.68
53.00	30.795	35.23	90.00	24.650	58.80	156.00	16.530	89.95
54.00	30.690	35.63	91.00	24.520	59.30	159.00	16.350	90.64
55.00	30.600	35.98	92.00	24.350	59.95	160.00	16.325	90.73
56.00	30.470	36.48	93.00	24.175	60.62	162.00	16.200	91.21
57.00	30.285	37.19	94.00	24.000	61.29	164.00	16.110	91.56
58.00	30.100	37.90	95.00	23.875	61.77	166.00	15.975	92.07
59.00	29.900	38.66	96.00	23.725	62.35	168.00	15.850	92.55
60.00	29.735	39.30	102.27	22.675	66.38	170.00	15.775	92.84
61.00	29.580	39.89	103.00	22.580	66.74	172.00	15.720	93.05
62.00	29.430	40.47	104.00	22.360	67.58	174.00	15.680	93.21
63.00	29.285	41.02	105.00	22.189	68.24	176.00	15.600	93.51
64.00	29.150	41.54	106.00	21.980	69.04	178.00	15.450	94.09
65.00	29.030	42.00	108.32	21.460	71.04	180.00	15.400	94.28
66.00	28.880	42.58	110.18	21.210	71.99	182.00	15.400	94.28
67.00	28.680	43.34	112.00	20.940	73.03	184.00	15.400	94.28
68.00	28.460	44.19	114.00	20.670	74.07	186.00	15.350	94.47
69.00	28.250	44.99	116.30	20.310	75.45	188.30	15.250	94.85
70.00	28.100	45.57	118.40	20.000	76.64	190.00	15.250	94.85
71.00	27.955	46.12	120.00	19.865	77.15	192.00	15.250	94.85
72.00	27.800	46.72	122.52	19.430	78.82	194.00	15.250	94.85
73.00	27.700	47.10	124.32	19.200	79.70	196.30	15.135	95.30
75.00	27.350	48.44	126.00	19.020	80.39	198.00	14.990	95.85
76.00	27.175	49.12	128.00	18.785	81.30	200.00	14.930	96.08
77.00	26.900	50.17	130.20	18.600	82.01	202.00	14.910	96.16
78.00	26.720	50.86	132.00	18.380	82.85	204.00	14.850	96.39
79.00	26.540	51.55	134.00	18.165	83.67	206.00	14.850	96.39
80.00	26.390	52.13	136.00	17.910	84.65	208.00	14.850	96.39
81.00	26.250	52.66	138.00	17.720	85.38	210.00	14.850	96.39
82.00	26.100	53.24	140.30	17.525	86.13			
83.00	25.940	53.85	142.00	17.400	86.61			

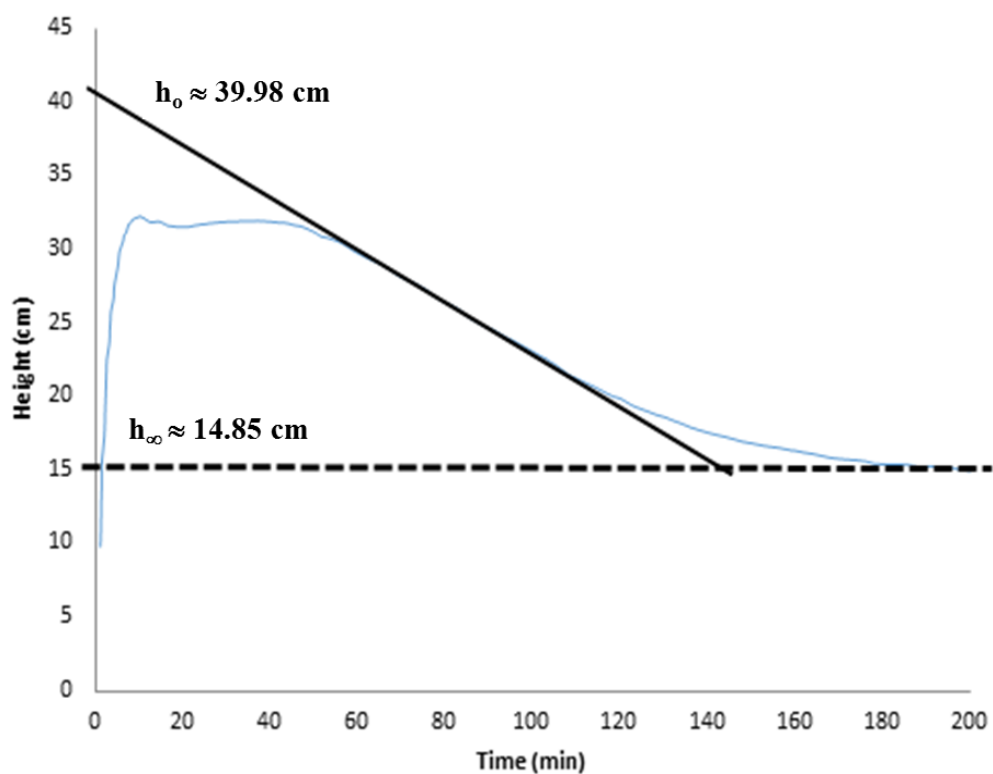


Figure 4.8 Extrapolation of h to zero time (h_0 at $t = 0$) for ϵ -caprolactone polymerisation using 0.1 mol % $\text{Sn}(\text{Oct})_2$ as initiator at 130°C .

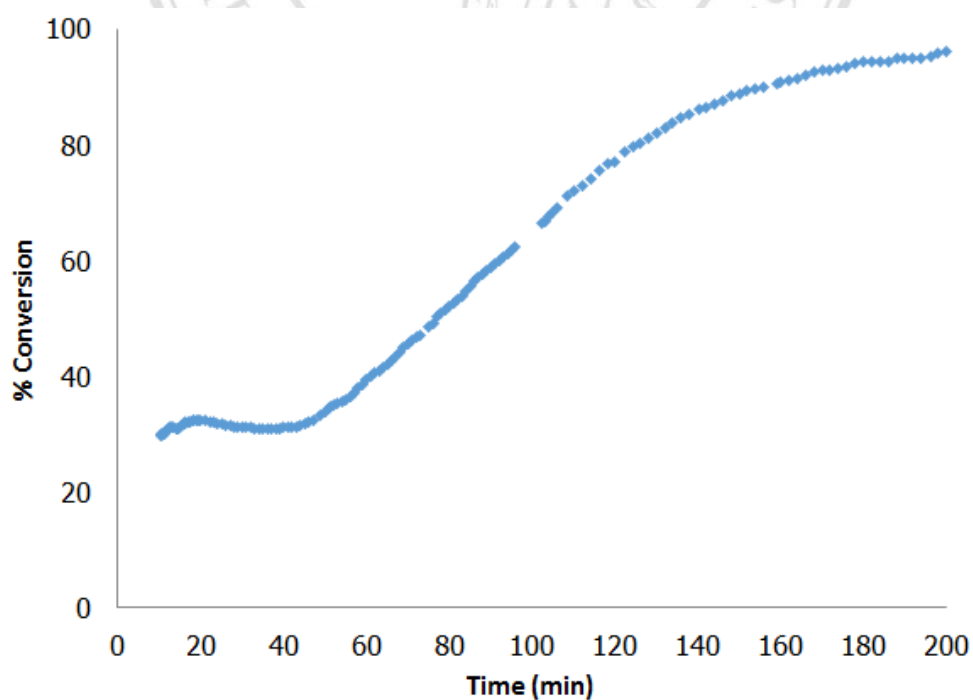


Figure 4.9 Kinetic profile from dilatometry of % conversion against time for ϵ -caprolactone using 0.1 mol % $\text{Sn}(\text{Oct})_2$ as initiator at 130°C .

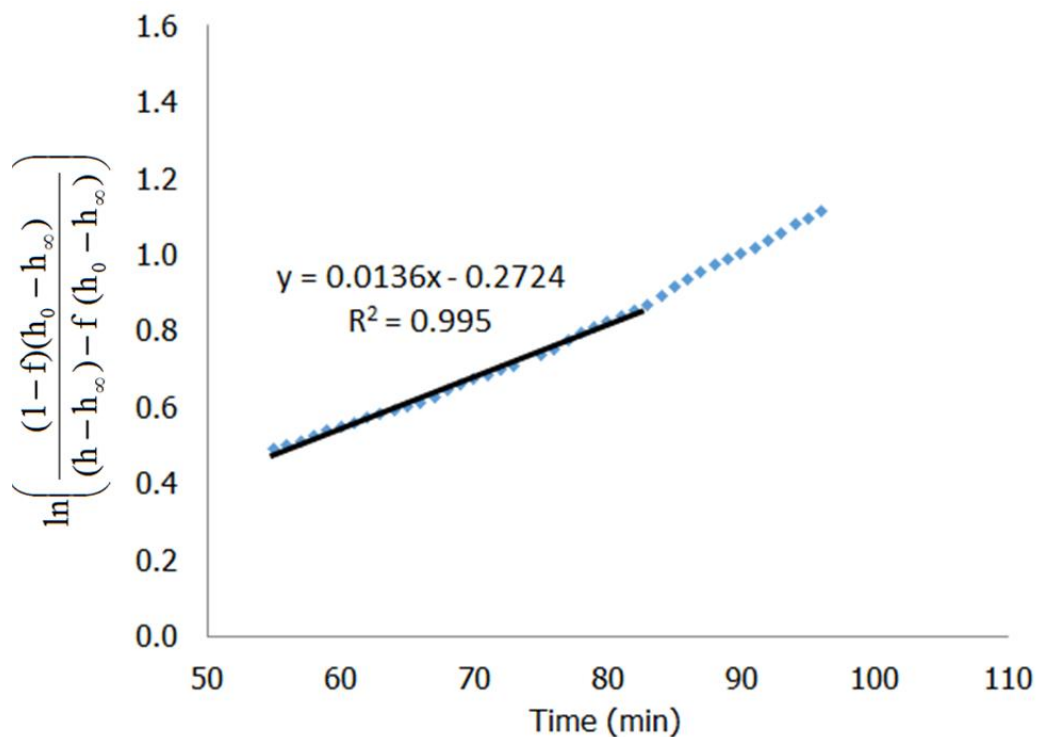


Figure 4.10 First-order rate plot from dilatometry for ϵ -caprolactone using 0.1 mol % $\text{Sn}(\text{Oct})_2$ as initiator at 130 °C.

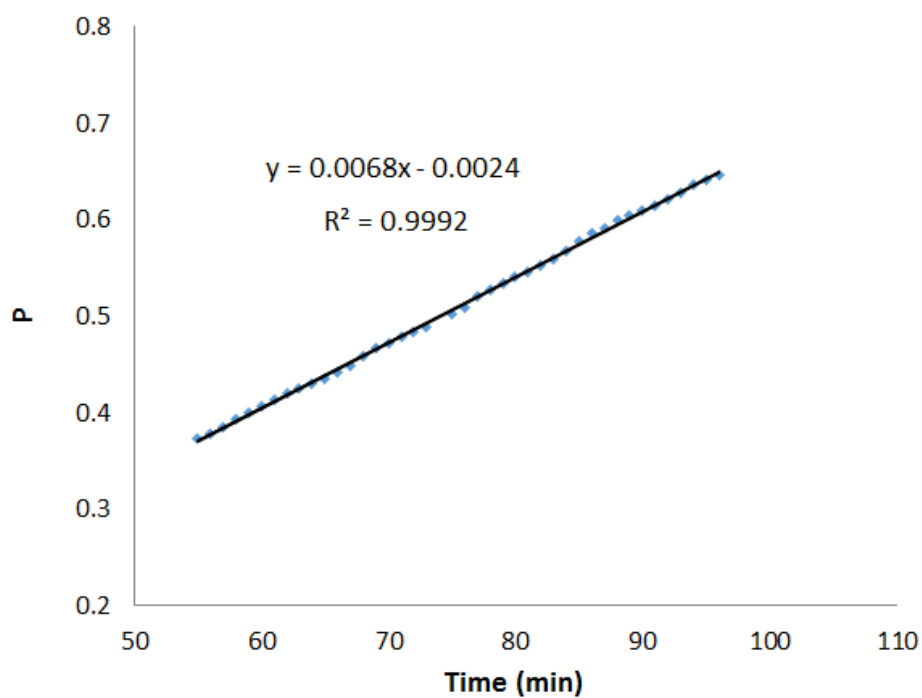


Figure 4.11 Zero-order rate plot from dilatometry for ϵ -caprolactone using 0.1 mol % $\text{Sn}(\text{Oct})_2$ as initiator at 130 °C.

Table 4.4 Dilatometry data of ϵ -caprolactone polymerisation at 130 °C using 0.1 mol % mixture initiator (Sn(Oct)₂ / DEG) as initiator.

Weight of ϵ -caprolactone = 14.6081 g h_0 (from extrapolation) = 33.73 cm
 Weight of Sn(Oct)₂ / DEG = 0.0815 g % Yield = 95.75
 Capillary diameter = 0.180 cm Residual monomer (f) = 0.042

Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion
1.28	8.775		8.25	30.285		22.00	29.750	17.73
1.35	9.000		8.42	30.470		23.00	29.420	19.20
1.46	11.475		9.00	30.635		23.30	29.250	19.96
1.59	13.300		9.20	30.820		24.00	29.175	20.30
2.12	14.870		9.40	30.930		25.00	29.030	20.94
2.24	16.280		9.56	31.050	Thermal	26.13	28.830	21.83
2.47	18.400		10.07	31.120	Equilibration	27.00	28.800	21.97
3.11	20.300		10.30	31.240		28.00	28.650	22.64
3.25	21.250		11.00	31.340		29.00	28.540	23.13
3.38	22.150		11.30	31.420		30.00	28.375	23.86
3.56	23.150		12.00	31.500		31.16	28.020	25.44
4.07	23.720	Thermal	12.30	31.550		32.05	27.690	26.91
4.21	24.440	Equilibration	13.00	31.550	9.71	33.30	26.900	30.43
4.34	25.040		13.30	31.530	9.80	34.00	26.530	32.08
4.58	25.900		14.00	31.485	10.00	35.00	25.950	34.67
5.10	26.300		14.30	31.430	10.25	36.00	25.470	36.80
5.25	26.720		15.00	31.380	10.47	37.00	25.050	38.68
5.43	27.225		15.30	31.275	10.94	38.05	24.420	41.48
6.00	27.600		16.00	31.190	11.32	39.10	23.950	43.58
6.11	27.900		16.30	31.075	11.83	40.00	23.600	45.14
6.24	28.180		17.00	31.000	12.16	41.08	23.140	47.19
6.40	28.600		17.30	30.900	12.61	42.00	22.900	48.26
6.53	28.900		18.00	30.825	12.94	43.09	22.600	49.59
7.06	29.100		18.30	30.790	13.10	44.04	22.320	50.84
7.28	29.500		19.00	30.760	13.23	45.22	21.990	52.31
7.40	29.670		19.30	30.625	13.84	46.00	21.800	53.16
7.56	29.910		20.00	30.490	14.44	47.00	21.430	54.80
8.12	30.120		21.00	30.100	16.17	48.15	21.050	56.50

Table 4.4 (Continued).

Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion
49.00	20.950	56.94	86.00	16.415	77.15	144.51	12.890	92.86
50.00	20.950	56.94	87.00	15.920	79.36	146.00	12.910	92.77
51.00	20.990	56.77	88.00	15.500	81.23	148.00	12.910	92.77
52.00	20.990	56.77	89.00	15.170	82.70	150.20	12.680	93.79
53.10	20.950	56.94	90.20	14.835	84.19	154.45	12.235	95.77
54.07	20.880	57.26	91.00	14.750	84.57	158.00	12.340	95.31
55.12	20.775	57.72	92.44	14.500	85.68	161.00	12.400	95.04
56.05	20.680	58.15	93.18	14.400	86.13	162.00	12.350	95.26
57.00	20.570	58.64	94.00	14.240	86.84	164.00	12.450	94.82
58.20	20.370	59.53	95.00	13.950	88.13	166.00	12.450	94.82
59.10	20.270	59.97	96.00	13.615	89.63	168.00	12.355	95.24
60.00	20.170	60.42	97.00	13.260	91.21	170.00	12.200	95.93
61.00	20.020	61.09	98.00	13.000	92.37	172.20	12.140	96.20
62.05	19.915	61.56	99.00	12.875	92.92	174.15	12.325	95.37
63.00	19.850	61.84	100.00	12.875	92.92	176.00	12.585	94.22
64.00	19.815	62.00	102.00	12.875	92.92	178.00	12.650	93.93
65.00	19.760	62.25	104.00	12.875	92.92	180.52	12.820	93.17
66.15	19.710	62.47	106.00	12.875	92.92	182.20	12.850	93.03
67.00	19.685	62.58	108.00	12.715	93.64	184.46	12.900	92.81
68.40	19.400	63.85	110.00	12.850	93.03	186.00	12.870	92.95
69.00	19.350	64.07	112.00	12.910	92.77	188.45	12.795	93.28
70.12	19.190	64.79	114.20	12.860	92.99	191.20	12.440	94.86
71.00	19.080	65.28	116.00	12.800	93.26	192.00	12.385	95.11
74.00	18.700	66.97	119.12	13.080	92.01	194.20	12.345	95.28
75.00	18.570	67.55	120.00	13.080	92.01	196.00	12.385	95.11
76.00	18.450	68.08	122.00	13.080	92.01	198.00	12.500	94.59
77.19	18.285	68.82	124.00	13.080	92.01	200.00	12.750	93.48
78.07	18.140	69.46	126.48	13.020	92.28	204.00	12.630	94.01
79.00	18.020	70.00	128.00	13.150	91.70	206.00	12.575	94.26
80.00	17.865	70.69	130.00	13.285	91.10	208.00	12.620	94.06
81.15	17.650	71.65	133.00	13.210	91.43	211.38	12.490	94.64
82.20	17.450	72.54	134.00	13.150	91.70	212.00	12.490	94.64
83.10	17.340	73.03	138.00	12.770	93.39	214.00	12.160	96.11
84.00	17.180	73.74	140.00	12.770	93.39	216.50	11.890	97.31
85.35	16.600	76.33	142.15	12.650	93.93	219.00	12.220	95.84
						220.00	12.320	95.40

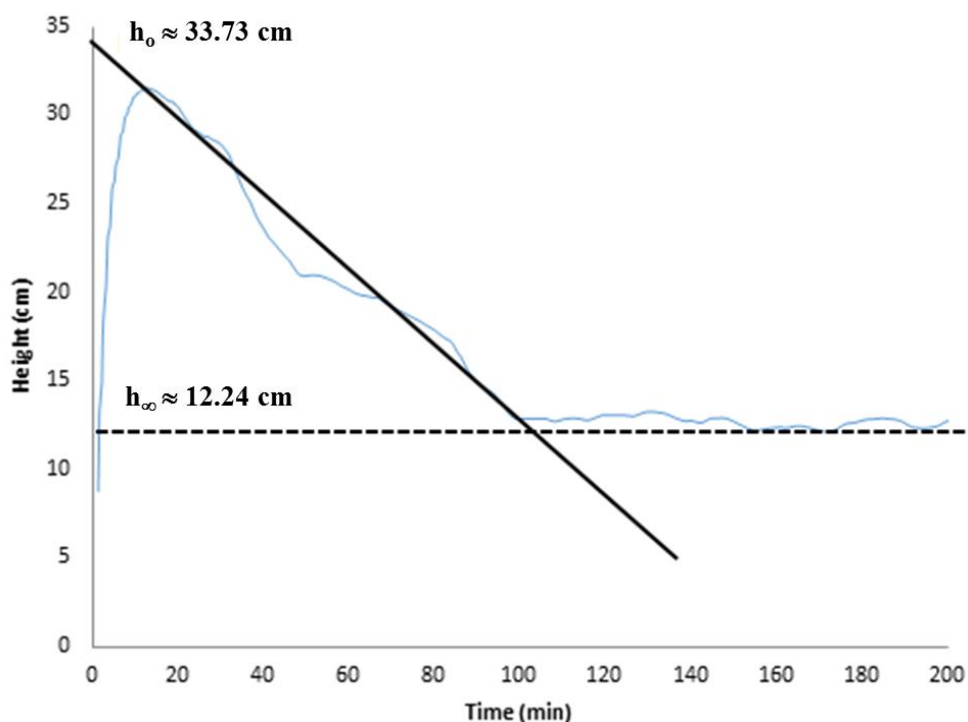


Figure 4.12 Extrapolation of h to zero time (h_0 at $t = 0$) for ϵ -caprolactone polymerisation using 0.1 mol % $\text{Sn}(\text{Oct})_2 / \text{DEG}$ as initiator at 130°C .

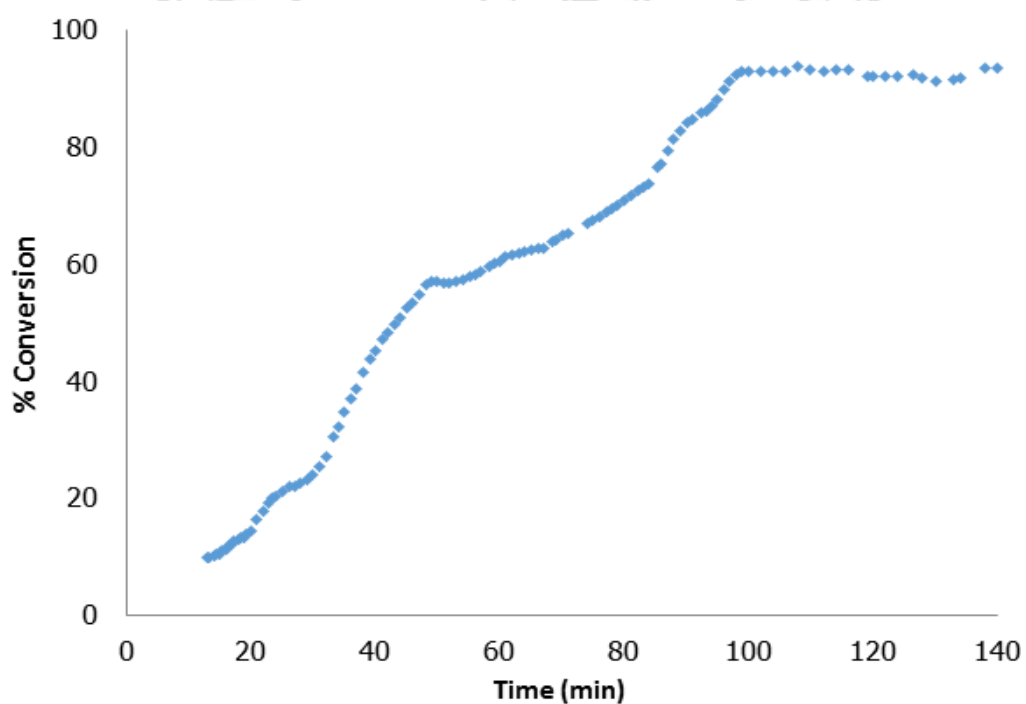


Figure 4.13 Kinetic profile from dilatometry of % conversion against time for ϵ -caprolactone using 0.1 mol % $\text{Sn}(\text{Oct})_2 / \text{DEG}$ as initiator at 130°C .

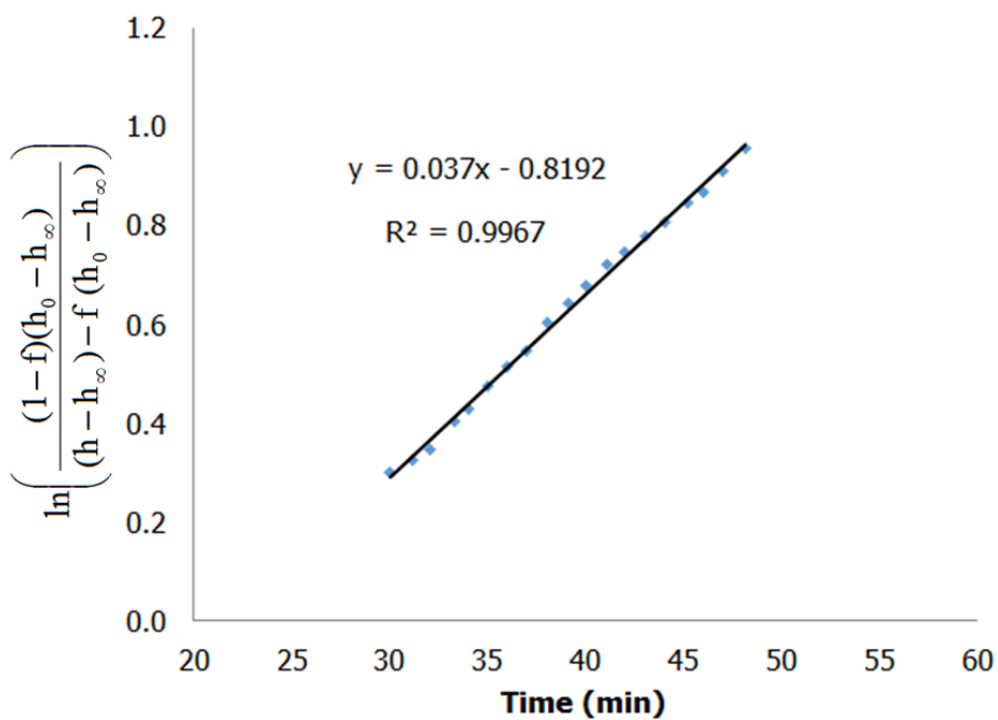


Figure 4.14 First-order rate plot from dilatometry for ϵ -caprolactone using 0.1 mol % $\text{Sn}(\text{Oct})_2$ / DEG as initiator at 130 °C.

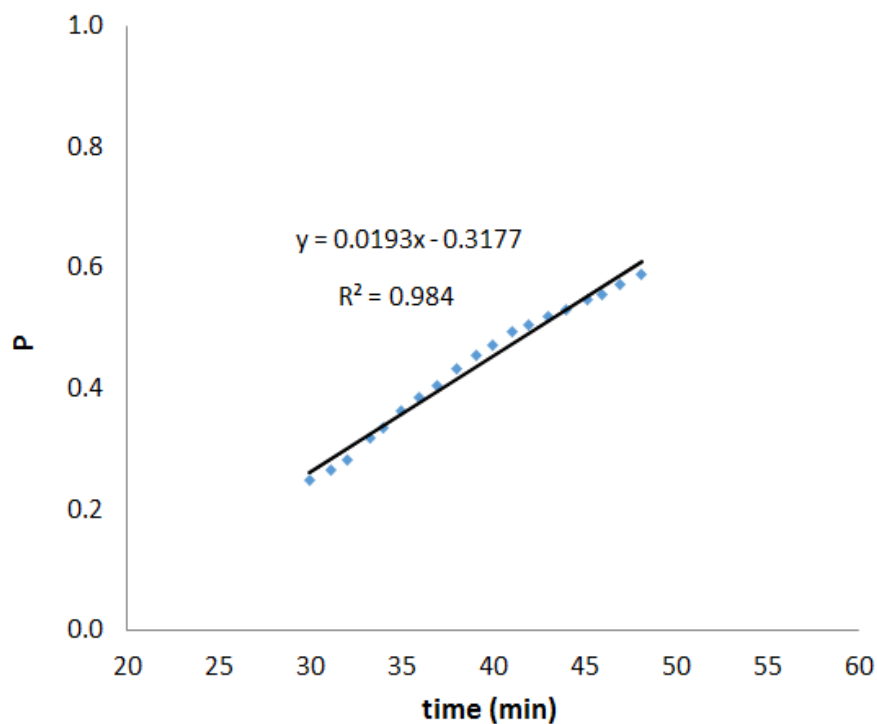


Figure 4.15 Zero-order rate plot from dilatometry for ϵ -caprolactone using 0.1 mol % $\text{Sn}(\text{Oct})_2$ / DEG as initiator at 130 °C.

Table 4.5 Dilatometry data of ϵ -caprolactone polymerisation at 130 °C using 0.1 mol % mixture initiator (Sn(Oct)₂ / EG) as initiator.

Weight of ϵ -caprolactone = 14.6008 g h_0 (from extrapolation) = 38.98 cm

Weight of Sn(Oct)₂ / EG = 0.0796 g % Yield = 99.71

Capillary diameter = 0.180 cm Residual monomer (f) = 0.003

Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion
1.23	8.650		8.01	29.280		22.00	30.863	30.57
1.32	9.900		8.22	29.470		23.00	30.775	30.90
1.41	11.360		8.36	29.640		24.00	30.650	31.37
1.53	12.985		8.53	29.760		25.00	30.500	31.93
2.12	15.250		9.12	29.883		26.30	30.260	32.84
2.24	16.520		9.33	29.995		27.00	30.210	33.03
2.38	17.770		9.56	30.150		28.00	29.980	33.89
2.52	19.100		10.36	30.320	Thermal	29.15	29.700	34.95
3.04	20.030		11.00	30.420	Equilibration	30.00	29.520	35.63
3.14	20.880		11.30	30.525		31.00	29.200	36.83
3.34	21.065	Thermal	12.00	30.600		32.14	28.890	38.00
4.03	23.650	Equilibration	12.30	30.660		33.00	28.690	38.75
4.15	24.190		13.00	30.690		34.10	28.380	39.92
4.30	24.770		14.00	30.782		35.00	28.175	40.69
4.43	25.300		14.30	30.820		36.00	27.883	41.79
4.58	25.780		15.00	30.840		37.00	27.590	42.89
5.12	26.250		15.30	30.860		38.00	27.275	44.08
5.31	26.750		16.00	30.875	30.52	39.05	26.900	45.49
5.44	27.070		16.30	30.860	30.58	40.20	26.440	47.22
5.56	27.350		17.00	30.845	30.64	41.00	26.225	48.03
6.09	27.625		17.30	30.850	30.62	42.04	25.870	49.37
6.24	27.940		18.00	30.850	30.62	43.00	25.600	50.39
6.40	28.190		18.30	30.850	30.62	44.00	25.350	51.33
7.07	28.640		19.00	30.850	30.62	45.00	25.000	52.65
7.26	28.900		19.30	30.845	30.64	46.00	24.710	53.74
7.36	29.000		20.00	30.850	30.62	47.00	24.385	54.96
7.46	29.130		21.00	30.920	30.35	48.00	24.050	56.22

Table 4.5 (Continued).

Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion
49.12	23.620	57.84	83.00	15.225	89.460	134.00	12.940	98.06
50.00	23.385	58.73	84.14	15.075	90.020	136.00	12.970	97.95
51.00	22.960	60.33	85.00	15.000	90.310	138.00	12.900	98.21
52.00	22.620	61.61	86.00	14.915	90.630	140.00	12.870	98.33
53.00	22.300	62.81	87.00	14.815	91.000	142.00	12.930	98.10
54.08	21.930	64.21	88.00	14.770	91.170	144.08	12.850	98.40
55.00	21.690	65.11	89.00	14.700	91.440	146.00	12.875	98.31
56.18	21.270	66.69	90.00	14.670	91.550	148.00	12.800	98.59
57.30	20.932	67.97	91.00	14.670	91.550	150.00	12.715	98.91
58.00	20.800	68.46	92.00	14.736	91.300	152.00	12.700	98.97
59.00	20.500	69.59	93.00	14.670	91.550	154.00	12.765	98.72
60.00	20.265	70.48	94.40	14.420	92.490	156.00	12.720	98.89
61.00	20.030	71.36	95.00	14.385	92.620	158.00	12.730	98.85
62.00	19.800	72.23	96.00	14.270	93.050	160.00	12.920	98.14
63.00	19.610	72.94	97.00	14.200	93.320	162.00	12.885	98.27
64.00	19.420	73.66	98.00	14.150	93.510	164.00	12.870	98.33
65.00	19.100	74.87	99.00	14.150	93.510	166.00	12.860	98.36
66.06	18.720	76.30	100.00	14.150	93.510	168.00	12.770	98.70
67.28	18.270	77.99	102.00	13.950	94.260	170.00	12.785	98.65
68.00	18.150	78.44	105.00	13.690	95.240	172.00	12.860	98.36
69.00	17.810	79.72	106.00	13.640	95.430	174.00	12.810	98.55
70.00	17.470	81.00	108.00	13.510	95.920	176.00	12.720	98.89
71.00	17.200	82.02	110.00	13.410	96.290	178.00	12.700	98.97
72.10	16.925	83.06	112.00	13.260	96.860	180.53	12.780	98.67
73.00	16.765	83.66	114.00	13.240	96.930	182.00	12.700	98.97
74.00	16.550	84.47	116.00	13.300	96.710	184.00	12.660	99.12
75.00	16.370	85.15	118.00	13.300	96.710	186.00	12.640	99.19
76.00	16.215	85.73	120.00	13.210	97.050	188.00	12.545	99.55
77.00	16.070	86.28	122.00	13.185	97.140	190.00	12.590	99.38
78.00	15.965	86.67	124.00	13.120	97.390	192.00	12.535	99.59
79.00	15.925	86.82	126.30	13.140	97.310	194.00	12.500	99.72
80.00	15.736	87.53	128.00	13.050	97.650	196.00	12.585	99.40
81.00	15.550	88.23	130.15	12.990	97.870	198.00	12.625	99.25
82.00	15.400	88.80	132.00	13.000	97.840	200.00	12.690	99.00

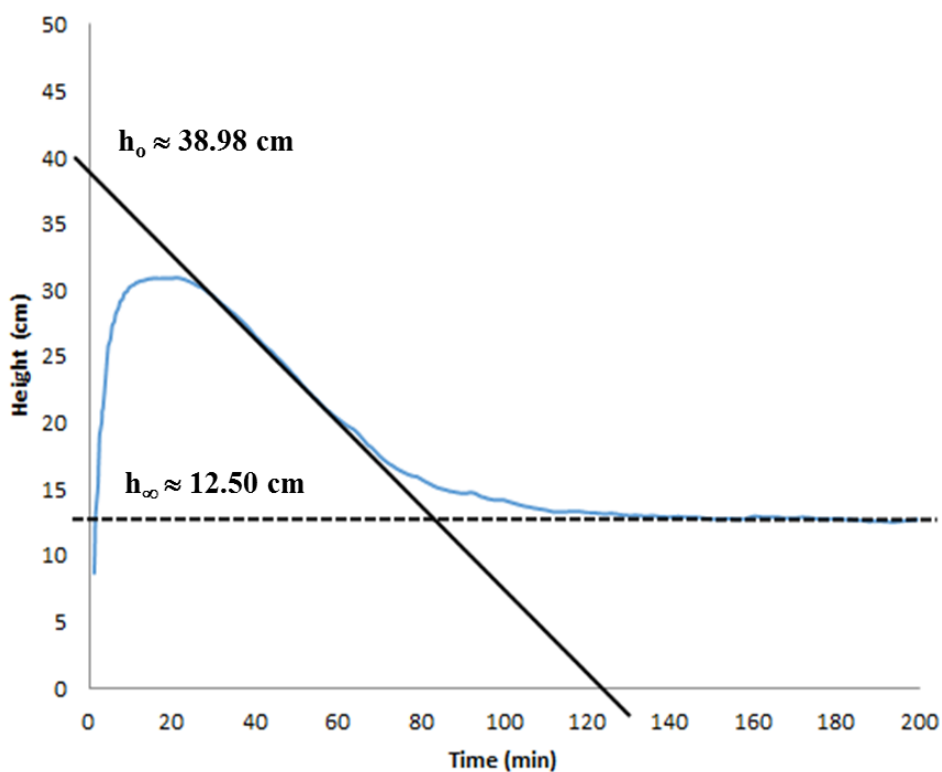


Figure 4.16 Extrapolation of h to zero time (h_0 at $t = 0$) and at constant height (h_∞) for ϵ -caprolactone polymerisation using 0.1 mol % $\text{Sn}(\text{Oct})_2 / \text{EG}$ as initiator at 130°C .

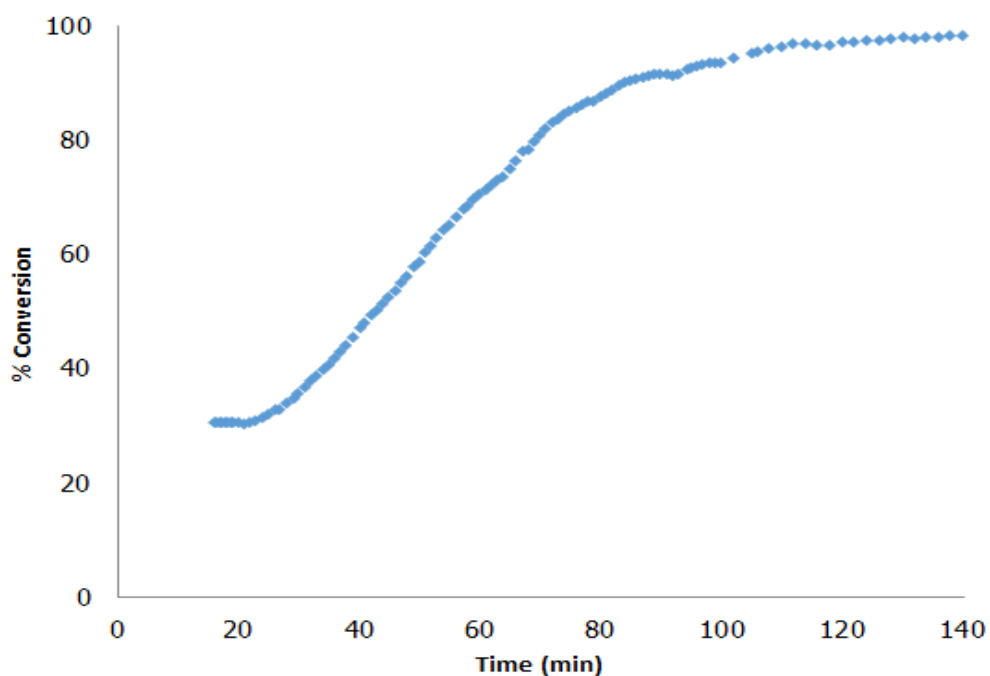


Figure 4.17 Kinetic profile from dilatometry of % conversion against time for ϵ -caprolactone using 0.1 mol % $\text{Sn}(\text{Oct})_2 / \text{EG}$ as initiator at 130°C .

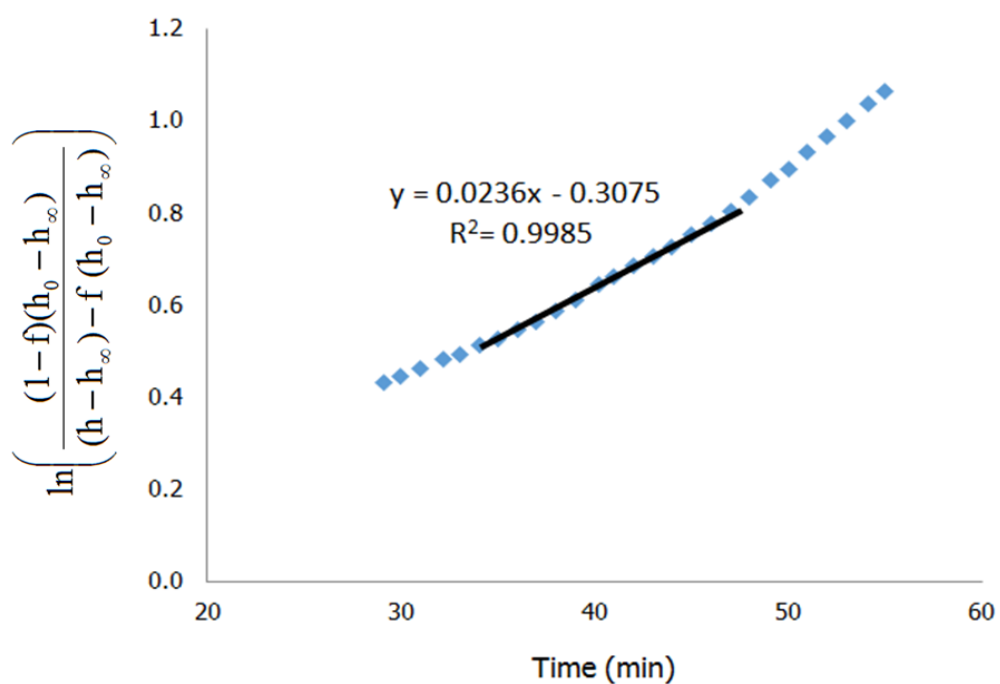


Figure 4.18 First-order rate plot from dilatometry for ϵ -caprolactone using 0.1 mol % $\text{Sn}(\text{Oct})_2$ / EG as initiator at 130 °C.

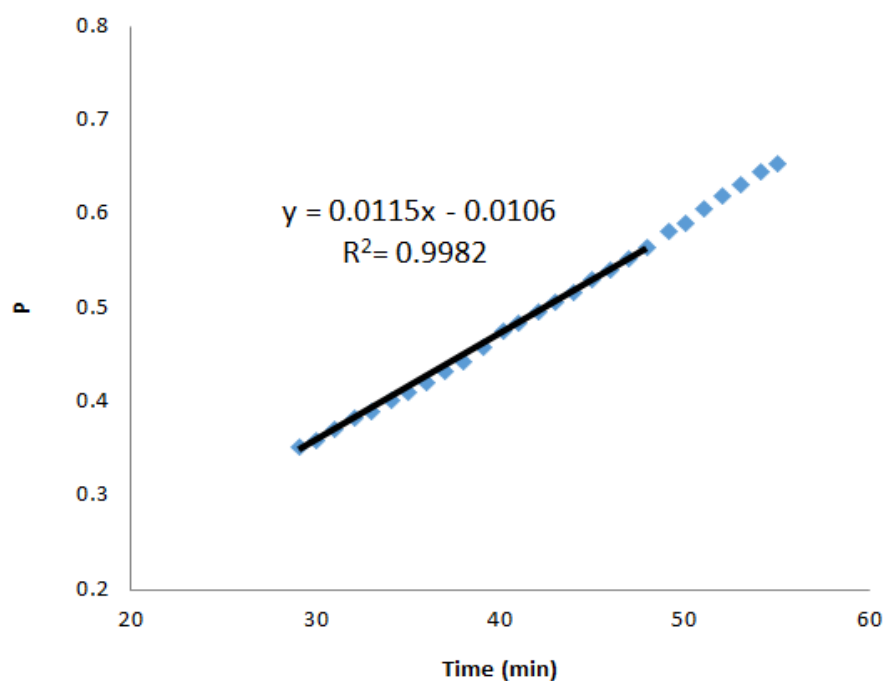


Figure 4.19 Zero-order rate plot from dilatometry for ϵ -caprolactone using 0.1 mol % $\text{Sn}(\text{Oct})_2$ / EG as initiator at 130 °C.

Table 4.6 Dilatometry data of ϵ -caprolactone polymerisation at 130 °C using 0.1 mol % [Sn(Oct)]₂DEG as initiator.

Weight of ϵ -caprolactone = 14.6070 g h_0 (from extrapolation) = 37.67 cm

Weight of [Sn(Oct)]₂DEG = 0.0811 g % Yield = 90.75

Capillary diameter = 0.180 cm Residual monomer (f) = 0.093

Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion
1.47	8.640		8.42	28.415		20.52	29.715	28.11
1.54	9.550		9.10	28.700		21.10	29.585	28.57
2.06	11.175		9.25	28.823		21.30	29.465	28.99
2.20	13.100		9.44	28.990		21.50	29.310	29.54
2.35	14.500		10.06	29.150		22.06	29.227	29.84
2.48	15.650		10.19	29.260		22.26	29.150	30.11
3.02	16.950		10.35	29.335		22.41	29.100	30.28
3.18	18.175		10.52	29.417	Thermal	23.05	29.100	30.28
3.30	19.100		11.10	29.545	Equilibration	23.37	29.145	30.13
3.40	19.720		11.58	29.765		24.00	29.200	29.93
3.50	19.410	Thermal	12.17	29.830		24.30	29.250	29.75
4.04	21.140	Equilibration	12.38	29.860		25.00	29.300	29.58
4.14	21.780		13.16	29.925		25.30	29.375	29.31
4.30	21.500		13.55	29.990		26.00	29.430	29.12
5.00	23.800		14.16	30.040		26.30	29.465	28.99
5.15	24.300		14.50	30.112		27.00	29.520	28.80
5.30	24.810		15.13	30.180		27.30	29.520	28.80
5.47	25.300		15.35	30.235		28.00	29.510	28.84
6.00	25.800		16.00	30.295		28.30	29.500	28.87
6.32	26.450		16.48	30.395	25.71	29.00	29.485	28.92
6.46	26.700		18.16	30.300	26.04	29.30	29.465	28.99
7.06	27.100		18.56	30.235	26.27	30.00	29.415	29.17
7.20	27.300		19.17	30.215	26.34	31.00	29.200	29.93
7.33	27.570		19.35	30.115	26.70	32.00	28.873	31.09
7.46	27.730		19.51	30.075	26.84	33.00	28.430	32.65
8.06	27.980		20.09	29.975	27.19	34.00	27.900	34.52
8.25	28.215		20.27	29.890	27.49	35.00	27.400	36.29

Table 4.6 (Continued).

Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion
36.00	27.040	37.56	72.00	18.020	69.44	76.00	16.960	73.18
37.00	26.910	38.02	73.00	17.770	70.32	77.00	16.810	73.71
38.00	26.870	38.17	74.00	17.500	71.28	78.00	16.720	74.03
39.00	26.850	38.24	75.00	17.180	72.41	79.00	16.630	74.35
40.00	26.780	38.48	76.00	16.960	73.18	80.00	16.530	74.70
41.15	26.550	39.30	77.00	16.810	73.71	81.00	16.450	74.99
42.00	26.320	40.11	78.00	16.720	74.03	82.00	16.390	75.20
43.00	25.900	41.59	79.00	16.630	74.35	83.00	16.300	75.52
44.00	25.400	43.36	80.00	16.530	74.70	84.00	16.200	75.87
45.00	24.870	45.23	81.00	16.450	74.99	85.14	16.000	76.58
46.00	24.490	46.58	82.00	16.390	75.20	86.00	15.870	77.04
47.00	24.250	47.42	83.00	16.300	75.52	87.00	15.675	77.73
48.00	24.120	47.88	84.00	16.200	75.87	88.00	15.340	78.91
49.00	24.000	48.31	85.14	16.000	76.58	89.00	15.025	80.02
50.00	23.820	48.94	86.00	15.870	77.04	90.00	14.750	80.99
51.00	23.500	50.07	55.00	22.160	54.81	91.00	14.650	81.35
52.00	23.120	51.42	56.00	21.920	55.66	92.00	14.600	81.52
53.00	22.710	52.87	57.00	21.620	56.72	93.00	14.600	81.52
54.00	22.385	54.01	58.00	21.260	57.99	94.00	14.590	81.56
55.00	22.160	54.81	59.00	20.870	59.37	95.00	14.590	81.56
56.00	21.920	55.66	60.00	20.525	60.59	96.00	14.590	81.56
57.00	21.620	56.72	61.00	20.270	61.49	97.00	14.590	81.56
58.00	21.260	57.99	62.00	20.050	62.27	98.09	14.470	81.98
59.00	20.870	59.37	63.00	19.850	62.97	99.00	14.400	82.23
60.00	20.525	60.59	64.00	19.660	63.64	100.00	14.250	82.76
61.00	20.270	61.49	65.00	19.450	64.39	101.00	14.065	83.41
62.00	20.050	62.27	66.00	19.200	65.27	102.00	13.835	84.23
63.00	19.850	62.97	67.35	18.835	66.56	103.00	13.565	85.18
64.00	19.660	63.64	68.00	18.750	66.86	104.00	13.390	85.80
65.00	19.450	64.39	69.00	18.530	67.64	105.00	13.370	85.87
66.00	19.200	65.27	70.00	18.400	68.10	106.00	13.370	85.87
67.35	18.835	66.56	71.00	18.225	68.71	107.00	13.425	85.68
68.00	18.750	66.86	72.00	18.020	69.44	108.00	13.490	85.45
69.00	18.530	67.64	73.00	17.770	70.32	109.00	13.530	85.31
70.00	18.400	68.10	74.00	17.500	71.28	110.00	13.600	85.06
71.00	18.225	68.71	75.00	17.180	72.41	111.00	13.600	85.06

Table 4.6 (Continued).

Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion
112.00	13.600	85.06	132.18	12.590	88.63	162.00	12.600	88.59
113.00	13.540	85.27	133.00	12.350	89.48	165.00	11.900	91.07
114.00	13.450	85.59	134.15	12.190	90.04	168.00	12.150	90.18
115.00	13.325	86.03	135.00	12.240	89.86	170.00	12.320	89.58
116.00	13.100	86.82	136.00	12.300	89.65	172.00	12.480	89.02
117.00	12.850	87.71	137.00	12.420	89.23	174.00	12.480	89.02
118.00	12.670	88.34	138.00	12.500	88.95	176.00	12.330	89.55
119.00	12.650	88.42	139.00	12.590	88.63	178.00	11.860	91.21
120.00	12.730	88.13	140.22	12.620	88.52	180.00	11.970	90.82
121.00	12.780	87.96	141.35	12.670	88.34	182.00	12.100	90.36
122.00	12.860	87.67	142.00	12.670	88.34	184.00	12.320	89.58
123.00	12.920	87.46	143.00	12.670	88.34	186.00	12.340	89.51
124.00	12.920	87.46	144.18	12.420	89.23	188.00	12.250	89.83
125.00	12.990	87.21	145.38	12.370	89.40	190.00	11.760	91.56
126.00	13.050	87.00	146.00	12.300	89.65	192.00	11.600	92.13
127.00	13.070	86.93	148.00	11.985	90.77	194.00	11.730	91.67
128.00	13.095	86.84	150.00	12.150	90.18	196.00	11.910	91.03
129.00	13.095	86.84	153.00	12.420	89.23	198.00	12.090	90.39
130.28	12.920	87.46	156.00	12.630	88.49	200.00	12.250	89.83
131.10	12.820	87.81	159.00	12.630	88.49			

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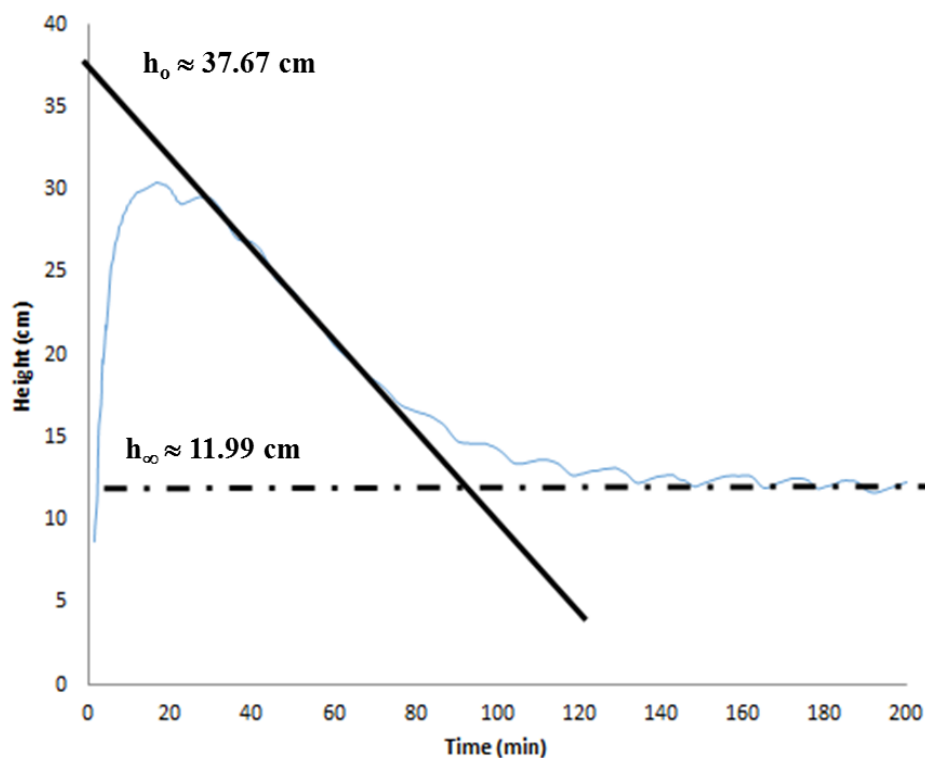


Figure 4.20 Extrapolation of h to zero time (h_0 at $t = 0$) for ϵ -caprolactone polymerisation using 0.1 mol % $[\text{Sn}(\text{Oct})_2]$ DEG as initiator at 130°C .

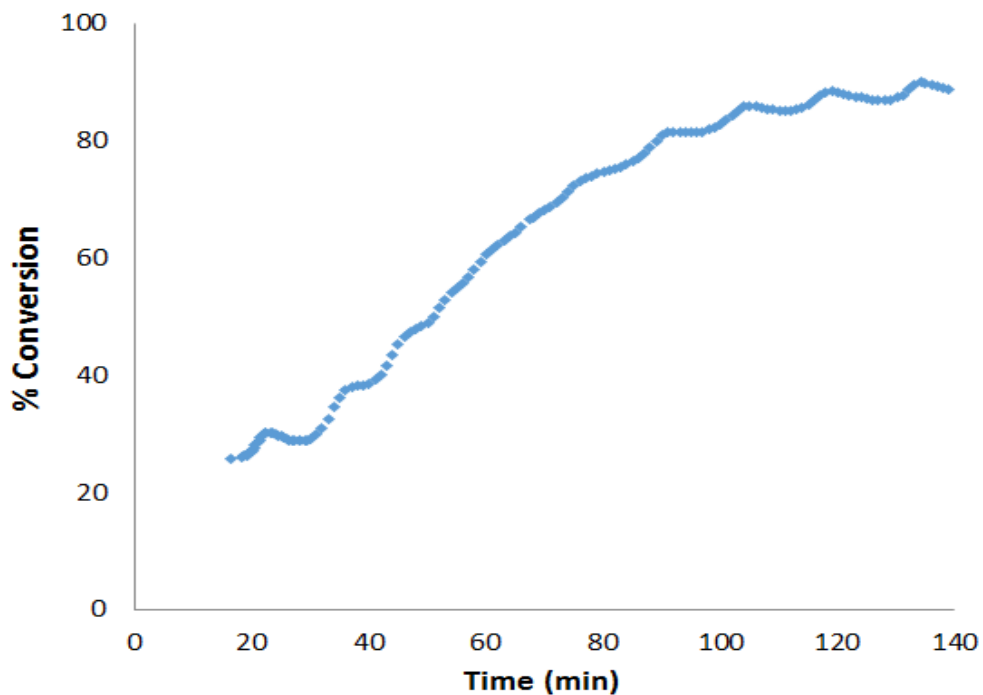


Figure 4.21 Kinetic profile from dilatometry of % conversion against time for ϵ -caprolactone using 0.1 mol % $[\text{Sn}(\text{Oct})_2]$ DEG as initiator at 130°C .

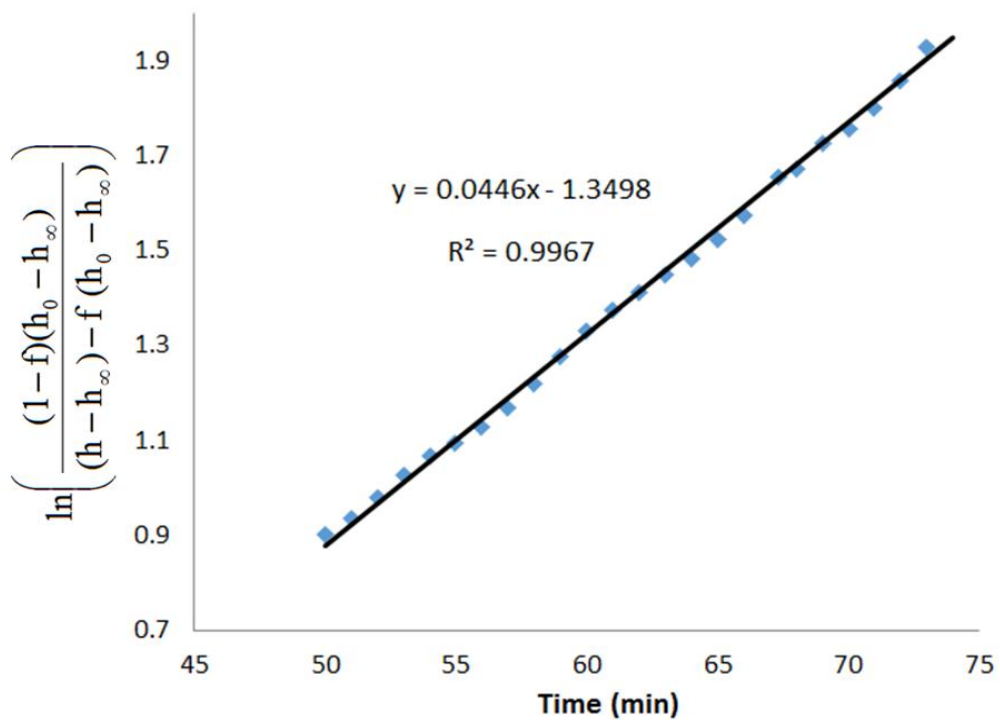


Figure 4.22 First-order rate plot from dilatometry for ϵ -caprolactone using 0.1 mol % $[\text{Sn}(\text{Oct})]_2$ DEG as initiator at 130 °C.

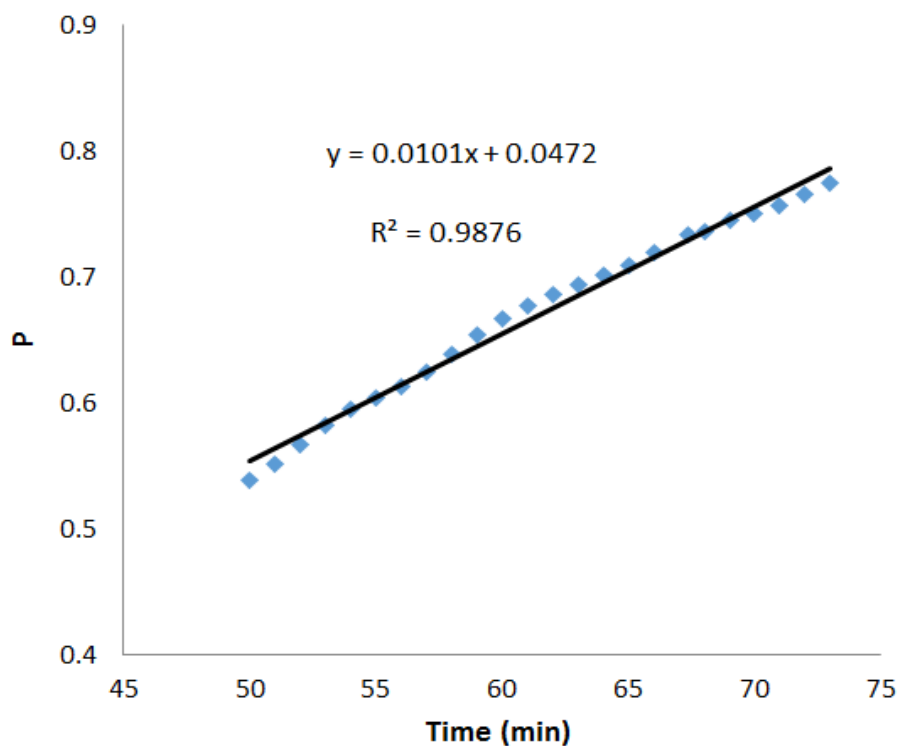


Figure 4.23 Zero-order rate plot from dilatometry for ϵ -caprolactone using 0.1 mol % $[\text{Sn}(\text{Oct})]_2$ DEG as initiator at 130 °C.

Table 4.7 Dilatometry data of ϵ -caprolactone polymerisation at 130 °C using 0.1 mol % [Sn(Oct)]₂EG as initiator.

Weight of ϵ -caprolactone	= 14.6150 g	h_0 (from extrapolation)	= 35.78 cm
Weight of [Sn(Oct)] ₂ EG	= 0.0751 g	% Yield	= 99.68
Capillary diameter	= 0.180 cm	Residual monomer (f)	= 0.003

Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion
1.09	10.200		7.33	29.020		21.00	29.810	24.53
1.20	11.900		7.52	29.150		22.00	29.635	25.25
1.30	13.325		8.04	29.200		23.00	29.333	26.49
1.45	15.450		8.18	29.300		24.00	29.070	27.57
1.55	16.670		8.50	29.410		25.00	28.850	28.47
2.10	18.250		9.08	29.470	Thermal	26.00	28.660	29.25
2.22	19.450		9.30	29.540	Equilibration	27.00	28.585	29.56
2.32	20.220		9.48	29.610		28.30	28.500	29.91
2.43	21.050		10.05	29.650		29.00	28.500	29.91
2.53	21.800		10.30	29.650		30.00	28.570	29.62
3.03	22.530		11.00	29.710		31.00	28.660	29.25
3.15	23.220	Thermal	11.30	29.770		32.00	28.645	29.32
3.29	24.050	Equilibration	12.00	29.810		33.00	28.560	29.67
3.40	24.550		12.30	29.810		34.00	28.450	30.12
3.50	24.975		13.00	29.870	24.28	35.42	28.240	30.98
4.01	25.420		13.30	29.850	24.37	36.00	28.170	31.27
4.14	25.875		14.00	29.870	24.28	37.23	27.900	32.38
4.27	26.310		14.30	29.920	24.08	38.00	27.775	32.89
4.40	26.700		15.00	29.920	24.08	39.00	27.300	34.84
4.53	27.025		15.30	29.970	23.87	40.00	26.850	36.69
5.07	27.350		16.00	30.000	23.75	41.00	26.400	38.54
5.36	28.090		17.00	30.070	23.46	42.20	25.670	41.54
5.52	28.320		17.30	30.700	20.87	43.00	25.400	42.65
6.23	28.750		18.44	29.990	23.79	44.00	25.120	43.80
6.36	28.900		19.10	30.040	23.58	45.00	24.800	45.11
6.47	28.950		19.30	30.040	23.58	46.00	24.620	45.85
6.58	29.020		20.00	29.970	23.87	47.00	24.425	46.66

Table 4.7 (Continued).

Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion	Time (min)	Height (cm)	% Conversion
48.00	24.200	47.58	77.00	16.820	77.90	112.00	12.680	94.91
49.00	23.950	48.61	78.30	16.650	78.60	114.24	12.480	95.73
50.00	23.750	49.43	79.00	16.480	79.30	116.00	12.350	96.27
51.00	23.590	50.09	80.00	16.335	79.90	118.00	12.330	96.35
52.00	23.270	51.40	81.00	16.220	80.37	120.00	12.260	96.64
53.00	23.050	52.30	82.00	16.040	81.11	122.00	12.260	96.64
54.15	22.840	53.17	83.45	15.785	82.16	124.00	12.260	96.64
55.00	22.610	54.11	84.00	15.735	82.36	126.47	12.330	96.35
56.00	22.330	55.26	85.30	15.470	83.45	128.00	12.340	96.31
57.00	22.140	56.04	86.00	15.340	83.98	130.00	12.350	96.27
58.00	21.930	56.91	87.00	15.080	85.05	132.30	12.330	96.35
59.22	21.580	58.34	88.00	14.835	86.06	134.17	12.200	96.89
60.00	21.450	58.88	89.00	14.580	87.11	136.00	12.000	97.71
61.00	21.185	59.97	90.00	14.420	87.76	138.00	11.650	99.14
62.00	20.900	61.14	91.00	14.280	88.34	140.00	11.590	99.39
63.00	20.500	62.78	92.00	14.110	89.04	143.00	11.520	99.68
64.00	20.130	64.30	93.00	14.040	89.32	144.00	11.520	99.68
65.00	19.700	66.07	94.00	13.930	89.78	146.00	11.520	99.68
66.00	19.280	67.79	95.00	13.830	90.19	148.00	11.550	99.56
67.30	18.800	69.77	96.00	13.750	90.52	150.00	11.600	99.35
68.00	18.650	70.38	97.00	13.700	90.72	155.00	11.835	98.38
69.00	18.380	71.49	98.00	13.670	90.85	160.00	11.870	98.24
70.00	18.180	72.31	99.00	13.550	91.34	171.49	11.490	99.80
71.00	17.960	73.22	100.00	13.520	91.46	178.44	11.680	99.02
72.00	17.720	74.20	102.00	13.490	91.58	180.00	11.740	98.78
73.00	17.550	74.90	104.00	13.420	91.87	185.00	11.500	99.76
74.00	17.340	75.77	106.00	13.375	92.06	190.00	11.470	99.88
75.00	17.140	76.59	108.00	13.250	92.57	195.00	11.550	99.56
76.00	16.971	77.28	110.00	13.000	93.60	200.00	11.710	98.90

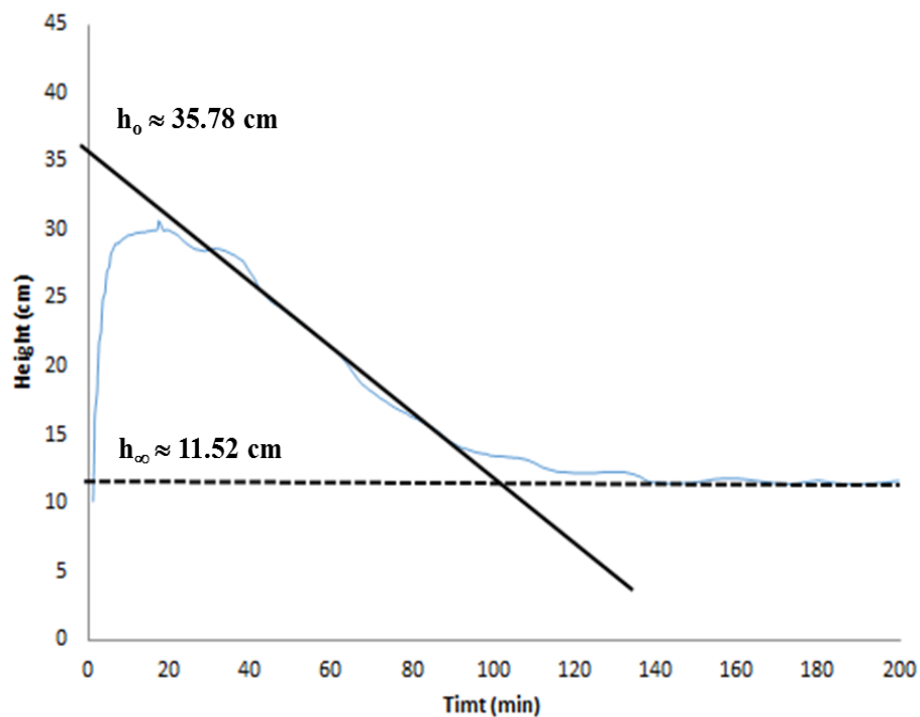


Figure 4.24 Extrapolation of h to zero time (h_0 at $t = 0$) for ϵ -caprolactone polymerisation using 0.1 mol % $[\text{Sn}(\text{Oct})]_2\text{EG}$ as initiator at 130°C .

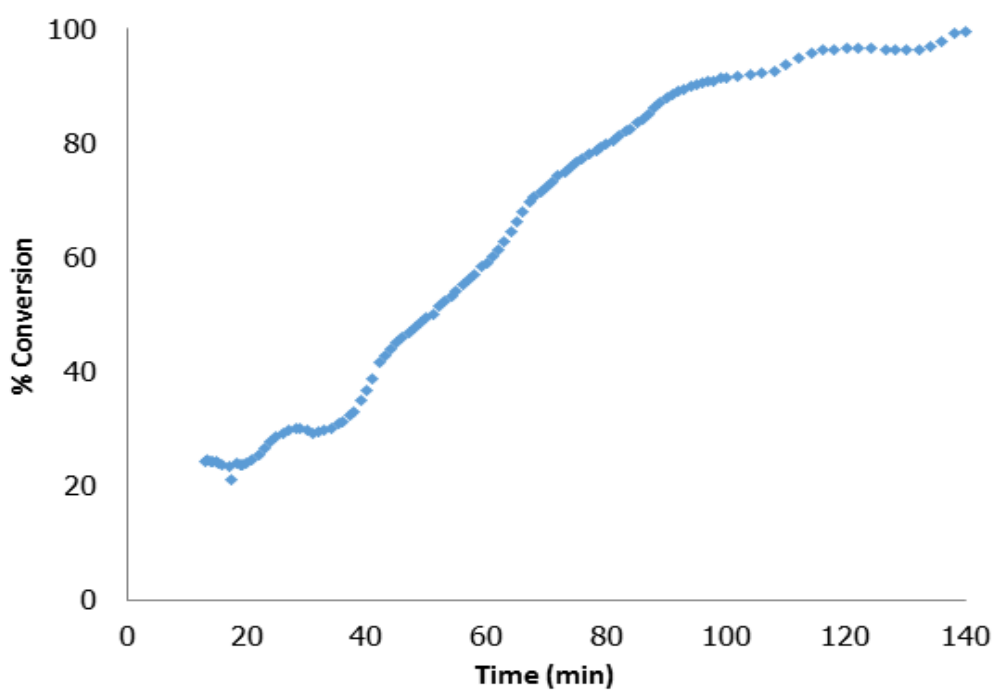


Figure 4.25 Kinetic profile from dilatometry of % conversion against time for ϵ -caprolactone using 0.1 mol % $[\text{Sn}(\text{Oct})]_2\text{EG}$ as initiator at 130°C .

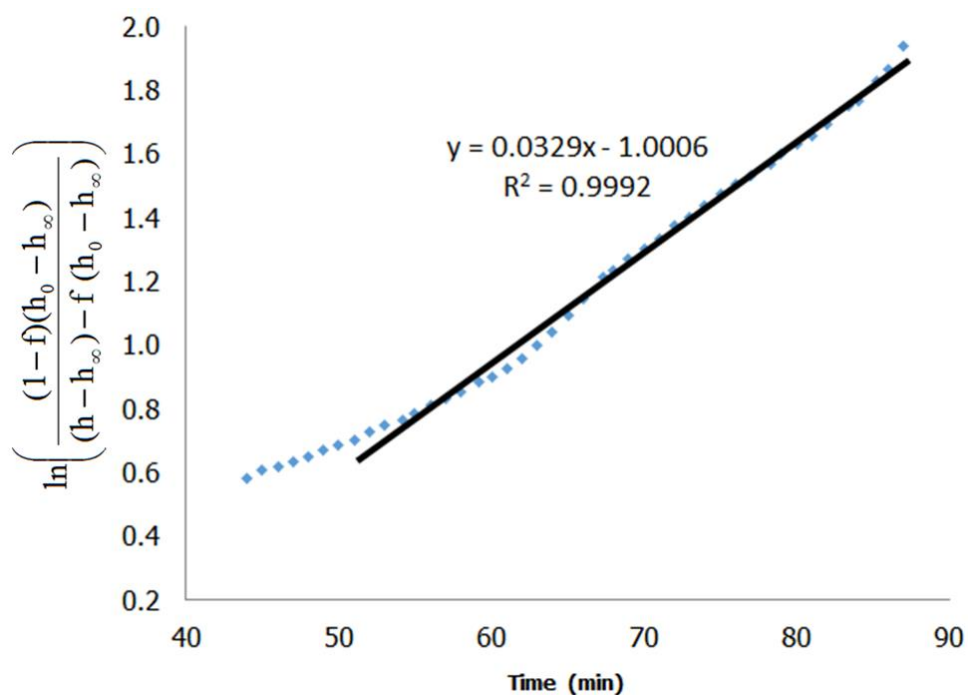


Figure 4.26 First-order rate plot from dilatometry for ϵ -caprolactone using 0.1 mol % $[\text{Sn}(\text{Oct})]_2\text{EG}$ as initiator at 130 °C.

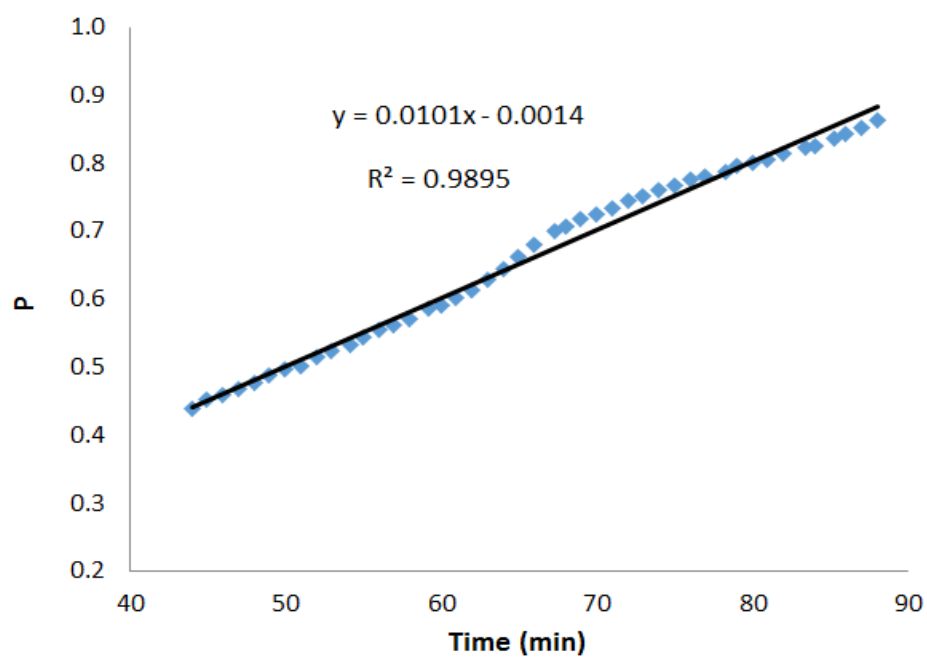


Figure 4.27 Zero-order rate plot from dilatometry for ϵ -caprolactone using 0.1 mol % $[\text{Sn}(\text{Oct})]_2\text{EG}$ as initiator at 130 °C.

Table 4.8 Summary of kinetic results for ϵ -caprolactone polymerisation using different liquid initiating systems at 130 °C.

Initiator	Concentration (mol %)	% Yield	First-order Rate Constant		Zero-order Rate Constant	
			k_1 (min ⁻¹)	R ²	k_0 (mol l ⁻¹ min ⁻¹)	R ²
Sn(Oct) ₂	0.1	96.4	0.014	0.995	0.059	0.999
Sn(Oct) ₂ /DEG *	0.2 / 0.1	95.8	0.037	0.997	0.168	0.984
Sn(Oct) ₂ /EG *	0.2 / 0.1	99.7	0.024	0.999	0.100	0.998
[Sn(Oct)] ₂ DEG **	0.1	90.7	0.045	0.997	0.088	0.988
[Sn(Oct)] ₂ EG **	0.1	99.7	0.033	0.999	0.088	0.990

The experimental data used for the kinetic calculation was taken from the 20-70 %

* Mixed initiators (tin(II) octoate / HOROH) with mol ratio = 2:1 → generates [Sn(Oct)]₂ORO *in situ*

** Initiators pre-prepared separately and used directly rather than generated *in situ*

The % yields, first-order rate constants, zero-order rate constants, and conversion ranges for the rate plots are summarized in Table 4.8. According to the literature, the polymerisation reaction in bulk is consistently described as being kinetically first-order with respect to the monomer concentration. However, as the results here have shown, the kinetic data in some cases fits a zero-order rate plot more closely than a first-order rate plot. The reasons for this are unclear but one possibility is that the deviation from first-order kinetics could be due to diffusion-controlled effects (e.g., Trommsdorf effect) as the viscosity of the system increases with % conversion. Increased viscosity also increases the viscous drag of the liquid meniscus on the glass surface of the dilatometer's capillary. Thus, there are both internal and external factors which may contribute towards a deviation from the expected first-order kinetics. Despite this, the first-order rate constants k_1 in Table 4.8 are still considered to be more reliable than the zero-order rate constants k_0 from a mechanistic point of view.

It is also significant to note in Table 4.8 that the first-order rate constants (k_1, min^{-1}) for the pre-prepared liquid initiators tended to be higher than for the corresponding $\text{Sn}(\text{Oct})_2$ / diol mixtures. This is as would be expected and shows the advantage of preparing the true initiator separately and using it directly rather than generating it *in situ* in an uncertain concentration.

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